Accurate prediction of ground motion using an hp-adaptive discontinuous Galerkin finite-element method (DG-FEM)

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## Introduction

## DG-FEM

- Spatial and time discretizations
- Tetrahedral meshing
- Boundary conditions
- Convergence study
- Computing aspects
- hp-adaptivity

### **EUROSEISTEST** Verification and Validation Project 3

- Model description
- Mesh building
- Numerical results

## Conclusions and perspectives

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  - Model description
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  - Numerical results

We investigate the potentials of DG-FEM for 3D seismic modeling

## Advantages

- Common to FEM
  - Arbitrary mesh geometry (fit of complex topographies)
  - Adaptive mesh to physical properties (h-adaptivity)
  - Local method suitable for parallel computing
- Specific to DG-FEM
  - Interpolation order mixing (p-adaptivity)
  - Discontinuous wavefield can be supported (fluid/solid interface)

## Drawbacks

• Computational cost, but...

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## Drawbacks

• Computational cost, but...

DG-FEM is competitive with other methods when complex topographies or extreme velocity contrasts are considered

# Introduction

## Characteristics of our approach

- 3D velocity-stress formulation in the time-domain
- Unstructured tetrahedral mesh (more flexible than hexahedral mesh)
- Nodal form of DG-FEM
- Constant physical properties per element
- Favour use of low interpolation orders for fine discretisation
- CPML absorbing boundary condition
- Intensive use of interpolation order mixing
  - Adapt the order according to elements size and medium properties
  - Lower order in the CPMLs to reduce the computational cost
- Centered flux (non-dissipative)

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# DG-FEM - Spatial and time discretizations

### Spatial discretization

- Discretize with non-overlapping and conformal tetrahedra
- Nodal form of DG-FEM (Hesthaven and Warburton, 2008)
- Approximate solution with Lagrangian polynomial basis functions and equidistant nodes



(a)  $P_0$  element with unique DOF. (b)  $P_1$  element element with 4 DOF. (c)  $P_2$  element with 10 DOF.

### Time discretization

Second order explicit leap-frog scheme

• Stability condition for the DG-FEM (Käser et al., 2008) gives  $\Delta t < \frac{1}{2d_i+1} \cdot \min_i \frac{2r_i}{V_{P}}$ 

- r<sub>i</sub> is the radius of the sphere inscribed in the element i
- V<sub>Pi</sub> the P-wave velocity
- d<sub>i</sub> the interpolation order of the cell

### The minimum required time step is imposed to all elements

# DG-FEM - Tetrahedral meshing

### Benefits of tetrahedral meshing

- Based on the Delaunay triangulation principle (Delaunay, 1934)
- Great flexibility in terms of design (complex shape) and refinement (local adaptivity)
- Efficient tetrahedral meshers are available (we use TETGEN)



# DG-FEM - Boundary conditions

### Free surface

- Explicit condition by changing locally the flux expression
- Introduce virtual cells which are exactly symmetric to the cells located on the free surface
- Inside these cells, impose identical velocity but opposite stress wavefield

### Absorbing condition

- Convolutional Perfectly Matched Layer (CPML) (Komatitsch and Martin, 2007)
- Unsplit formulation with memory variables
- Improve absorption of waves at grazing incidence
- In the CPML, the damping function is defined in the frequency domain as follows

$$s_{ heta} = \kappa_{ heta} + rac{d_{ heta}}{lpha_{ heta} + i\omega} \qquad orall heta \in \{x, y, z\}$$

with the angular frequency  $\omega$  and  $\kappa_\theta \geq 1$  and  $\alpha_\theta \geq 0$ 

• If  $\kappa_{\theta} = 1$  and  $\alpha_{\theta} = 0$ , one get the classical PML formulation (Berenger, 1994)

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# DG-FEM - Convergence study

### Eigen mode in a cube



Initial conditions + free surfaces = continual monochromatic signals

### Convergence rate



# DG-FEM - Computing aspects

### Parallelism

- Domain decomposition strategy, one subdomain = one CPU
- MPI communication between subdomains
- Efficient load balancing with mesh partitioning (METIS)
- Average parallelism efficiency of 80 %



### Possible bottle-neck

- Time step is common for all subdomains
- Dramatic effects of badly shaped elements
- Mitigate these negative effects with p-adaptivity

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# DG-FEM - hp-adaptivity

Interpolation order mixing : an efficient mean to mitigate effects of badly shaped tetrahedra

Downgrade order of badly shaped element = increase time step



Time step versus the element size for different interpolation orders with  $V_P = 6000$  m/s Grey curve :  $P_0$ ; blue curve :  $P_1$ ; red curve :  $P_2$ ; dashed line : interpolation order mixing

### Our 2-step refinement approach

- 1<sup>st</sup> step : Iterative mesh refinement (h-adaptivity)
  - based on medium properties and discretization target (3 cells / λ with P<sub>2</sub>)
  - repeated until required discretisation is reached

• 2<sup>nd</sup> step : adapt the interpolation order with an a priori error estimate (p-adaptivity)

$$\begin{array}{ll} P_2 & \text{if } \lambda/8 < \text{cell size} \\ P_1 & \text{if } \lambda/24 < \text{cell size} \leq \lambda/8 \\ P_0 & \text{if cell size} \leq \lambda/24 \end{array} \right\} \text{heuristic criteria}$$

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# EUROSEISTEST - Model description

### EUROSEISTEST Verification and Validation project

- Organized by CEA, LGIT, University of Thessaloniki and Institute Laue Langevin
- 10 modeling teams (FDM, FEM, SEM, DEM, DG-FEM and PSM)

### Model characteristics

- Sedimentary basin 30 km E-NE of Thessaloniki (Northern Greece)
- Low velocity in basin and high velocity bedrock

	P-wave velocity	S-wave velocity	Ratio V <sub>P</sub> / V <sub>S</sub>	Max. depth
Basin	from 1000 to 3027 m/s	from 200 to 848 m/s	from 5.00 to 3.57	411 m
Bedrock	from 4500 to 6144 $m/s$	from 2600 to 3444 m/s	from 1.73 to 1.78	8 km

- Ratio Max.  $V_S$  / Min.  $V_S = 17$
- High Poisson ratio in the basin
- Thin structures
- Double-couple source with max. frequency of 4 Hz ( $M_w = 1.3$ )

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# EUROSEISTEST - Model description



(a) View of the mesh in the plan xy at z = 0 m showing the P-wave velocity associated to each cell in the EUROSEISTEST model. The receivers are represented with numbered green triangles and the source epicenter with a yellow star. (b) Same with S-wave velocity associated to each cell. The direction of the cross-section AB is indicated with a white segment.

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# EUROSEISTEST - Mesh building

## Iterative mesh refinement (h-adaptivity)



(a) Cross section AB of the mesh at the first iteration of the h-refinement showing the S-wave velocity associated to each cell in the EUROSEISTEST model. (b) Same as (a) at the second iteration of the h-refinement. (c) Same as (a) at the sixth and last iteration of the h-refinement.

# EUROSEISTEST - Mesh building

## Interpolation order mixing (p-adaptivity)



(a) View of the mesh in the plan xy at z = 0 m showing the size of the elements (insphere radius) in the EUROSEISTEST model. (b) Same with interpolation order associated to each cell.  $P_2$  elements are represented in white,  $P_1$  in grey and  $P_0$  in black.

- The basin represents 1 % of the model and contains more than 70 % elements in the mesh
- 65.51 % P<sub>2</sub>, 34.36 % P<sub>1</sub> (with 31.51 % in CPML) and 0.13 % P<sub>0</sub> elements
- Interpolation order mixing plays an important role at the basin edges

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# EUROSEISTEST - Numerical results

## Comparison between DG-FEM and SEM



(a) Seismograms of  $v_x$  computed with DG-FEM (black line) and SEM (red line). (b) Same as (a) with  $v_z$ .

Perfect match between both solutions for receivers in bedrock (1 and 4)

### For other receivers

- for v<sub>z</sub> very good agreement
- for  $v_x$  good for short times but misfits are increasing with time

# **EUROSEISTEST - Numerical results**

## Model discretization

When looking closely at the free surface with a reduced velocity scale...



(a) View of the mesh in the plan xy at z = 0 m showing the P-wave velocity. (b) Same with S-wave velocity.

Due to constant properties per element, velocities at the free surface are higher than real values ( $V_P = 1000 \text{ m/s}$  and  $V_S = 200 \text{ m/s}$ )

 $\Rightarrow$  It may be the origins of the misfits at long times

# **EUROSEISTEST - Numerical results**

## Comparison between DG-FEM and SEM



(a) Peak Ground Velocity (PGV) map computed for the EUROSEISTEST modeling with DG-FEM. The receivers are represented with numbered white triangles and the source epicenter with a yellow star. (b) Same as (a) computed with SEM.

### Excellent agreement of the PGV maps between DG-FEM and SEM

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## Comparison between DG-FEM and SEM

If time permits, let's see a little movie of the ground motion...

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## Comparison between DG-FEM and SEM

### Mesh statistics

Method	Order	I <sub>min</sub>	I <sub>max</sub>	Nb elements	Nb DOF	Nb unknowns
DG-FEM	$P_2/P_1/P_0$	2.5 m	399.8 m	$16.3 imes10^6$	$131.6 imes10^6$	$1.31 imes10^9$
SEM	$P_4$	20.0 m	908.0 m	$1.4 imes10^{6}$	$91.7 imes10^{6}$	$0.27 imes10^9$

### **Computation times**

Method	Nb time steps	Nb procs	CPU time	Mem.	CPU type
DG-FEM	122 565	144	52h	26 GB	IBM E5420 2.5 Ghz
SEM	75 000	144	7h	25 GB	IBM E5420 2.5 Ghz

• Ratio DG-FEM CPU time / SEM CPU time is 7 (for similar accuracy)

- Number of unknowns is 4.8 times higher with DG-FEM
- Number of time steps is 1.6 times higher with DG-FEM
- In more complex media, DG-FEM should be more competitive...

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### Conclusions

- DG-FEM has great potentials for seismic modeling in highly heterogeneous media
- Designed an effective hp-adaptive scheme (CPU time reduced by one order of magnitude)
- Approach has been validated with the EUROSEISTEST Verification and Validation Project

### Perspectives

- Take into account anisotropy
- Allow for physical properties variation inside elements
  - Explore higher orders in space
  - Explore higher orders in time
- Implement visco-elastic rheologies (Käser et al., 2007)
- Wave propagation in fractured media
- Dynamic rupture (BenJemaa et al., 2007, 2009; de la Puente et al., 2009)
- Application of the method to Full Waveform Inversion (FWI)

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