a short lecture on

# The spectral-element method

by

Andreas Fichtner



Universiteit Utrecht

Department of Earth Sciences

QUantitative estimation of Earth's seismic sources and STructure

- originally developed in fluid dynamics (Patera, 1984)
- migrated to seismology in the early 1990's (Seriani & Priolo, 1991)
- major advantage: accurate modelling of interfaces and the free surface (with topography)



1. The weak form of the wave equation ...

... in 1D

$$\rho \ddot{u} - \frac{\partial}{\partial x} \left( \mu \frac{\partial}{\partial x} u \right) = f \qquad \frac{\partial}{\partial x} u(t,0) = \frac{\partial}{\partial x} u(t,L) = 0$$

strong form of the wave equation

------ PDE ------ -- B.C. (free surface in 3D) --



vibrating string of length L

$$\rho \ddot{u} - \frac{\partial}{\partial x} \left( \mu \frac{\partial}{\partial x} u \right) = f \qquad \frac{\partial}{\partial x} u(t,0) = \frac{\partial}{\partial x} u(t,L) = 0$$

strong form of the wave equation

$$\int_{0}^{L} \rho w \ddot{u} dx - \int_{0}^{L} w \frac{\partial}{\partial x} \left( \mu \frac{\partial}{\partial x} u \right) dx = \int_{0}^{L} w f dx$$

multiply with test function w(x) integrate over x from 0 to L

$$\rho \ddot{u} - \frac{\partial}{\partial x} \left( \mu \frac{\partial}{\partial x} u \right) = f \qquad \frac{\partial}{\partial x} u(t,0) = \frac{\partial}{\partial x} u(t,L) = 0$$

strong form of the wave equation

$$\int_{0}^{L} \rho w \ddot{u} dx - \int_{0}^{L} w \frac{\partial}{\partial x} \left( \mu \frac{\partial}{\partial x} u \right) dx = \int_{0}^{L} w f dx$$

multiply with test function w(x) integrate over x from 0 to L

$$\int_{0}^{L} \rho w \ddot{u} dx + \int_{0}^{L} \mu \left(\frac{\partial}{\partial x} w\right) \left(\frac{\partial}{\partial x} u\right) dx = \int_{0}^{L} w f dx$$

integrate by parts use the boundary conditions

#### Solving the weak form of the wave equation means

### to find a displacement field u(x,t) such that

$$\int_{0}^{L} \rho w \ddot{u} dx + \int_{0}^{L} \mu \left(\frac{\partial}{\partial x} w\right) \left(\frac{\partial}{\partial x} u\right) dx = \int_{0}^{L} w f dx$$

is satisfied for any differentiable test function w(x).

Find a displacement field u(x,t) such that

$$\int_{0}^{L} \rho w \ddot{u} dx + \int_{0}^{L} \mu \left(\frac{\partial}{\partial x} w\right) \left(\frac{\partial}{\partial x} u\right) dx = \int_{0}^{L} w f dx$$

is satisfied for any differentiable test function w(x).

# Why is this important to know ?

Find a displacement field u(x,t) such that

$$\int_{0}^{L} \rho w \ddot{u} dx + \int_{0}^{L} \mu \left(\frac{\partial}{\partial x} w\right) \left(\frac{\partial}{\partial x} u\right) dx = \int_{0}^{L} w f dx$$

is satisfied for any differentiable test function w(x).

# 1. The basis of many numerical techniques:

- Finite-element method (FEM)
- Spectral-element method (SEM)
- Discontinuous Galerkin method (DGM)



2. Free surface boundary condition is automatically satisfied BIG advantage!



- 2. Free surface boundary condition is automatically satisfied
  - **BIG advantage!** <u>Compare to finite-difference method:</u>





- 2. Free surface boundary condition is automatically satisfied
  - **BIG advantage!** <u>Compare to finite-difference method:</u>





2. Free surface boundary condition is automatically satisfied BIG advantage!

Correct free surface comes without any additional effort!



This makes accurate surface waves!

2. Spatial discretisation

## **SEM** in 1D: decomposition of the computational domain

- **1.** decompose the computational domain [0, L] into disjoint elements E<sub>i</sub>
- 2. consider integral element-wise



$$\int_{E_{i}} \rho w \ddot{u} dx + \int_{E_{i}} \mu \left(\frac{\partial}{\partial x} w\right) \left(\frac{\partial}{\partial x} u\right) dx = \int_{E_{i}} w f dx$$

$$E_{i}$$

## **SEM** in 1D: mapping to the reference interval

**3.** map each element to the reference interval [-1, 1]



$$\int_{E_{i}} \rho w \ddot{u} dx + \int_{E_{i}} \mu \left(\frac{\partial}{\partial x} w\right) \left(\frac{\partial}{\partial x} u\right) dx = \int_{E_{i}} w f dx$$

$$E_{i}$$



-1

#### SEM in 1D: mapping to the reference interval



$$\int_{-1}^{-1} \rho \le \ddot{u} \frac{dx}{dy} dy + \dots$$













# **SEM** in 1D: approximation by polynomials

- 4. Approximate u by Lagrange polynomials collocated at the GLL points
- 5. choose Lagrange polynomials also for the test function w

$$\int_{-1}^{-1} \rho w \ddot{u} \frac{dx}{dy} dy + \dots$$

$$\ell_{k}(y) u'(y, t) = \sum_{i=0}^{N} u_{i}(t) \ell_{i}(y)$$

#### **SEM** in 1D: The mass matrix

- 4. Approximate u by Lagrange polynomials collocated at the GLL points
- 5. choose Lagrange polynomials also for the test function w



6. The integral is approximated using Gauss-Lobatto-Legendre (GLL) quadrature.

Mass matrix is diagonal !!! Big advantage !!!

$$\int_{-1}^{-1} \rho \mathbf{w} \, \ddot{\mathbf{u}} \frac{dx}{dy} \, dy = \sum_{i=0}^{N} \left[ \int_{-1}^{1} \rho \, \ell_k \, \ell_i \, \frac{dx}{dy} \, dy \right] \ddot{\mathbf{u}}_i$$
$$\sum_{i=0}^{N} M_{ki} \, \ddot{\mathbf{u}}_i(t)$$
$$\mathbf{M} = \mathbf{mass matrix}$$

# SEM in 1D: A brief summary

$$\int_{E_i} \rho w \ddot{u} dx + \int_{E_i} \mu \left( \frac{\partial}{\partial x} w \right) \left( \frac{\partial}{\partial x} u \right) dx = \int_{E_i} w f dx$$

weak form, element-wise

- 1. mapping to the reference interval [-1,1]
- 2. polynomial approximation (GLL points)
- 3. numerical integration (GLL quadrature)



# SEM in 1D: A brief summary

$$\int_{E_{i}} \rho w \ddot{u} dx + \int_{E_{i}} \mu \left( \frac{\partial}{\partial x} w \right) \left( \frac{\partial}{\partial x} u \right) dx = \int_{E_{i}} w f dx \qquad \text{ver}$$

$$\int_{E_{i}} \rho w \ddot{u} dx + \int_{E_{i}} \mu \left( \frac{\partial}{\partial x} w \right) \left( \frac{\partial}{\partial x} u \right) dx = \int_{E_{i}} w f dx \qquad \text{repeat}$$

$$\int_{E_{i}} M_{ki} \ddot{u}_{i}(t) + \sum_{i=0}^{N} K_{ki} \ddot{u}_{i} = f_{i}$$

$$\int_{E_{i}} M_{ki} \ddot{u}_{i}(t) + \sum_{i=0}^{N} K_{ki} \ddot{u}_{i} = f_{i}$$

$$\int_{E_{i}} f_{i} discrete \text{ force vector}$$

weak form, element-wise

repeat this for the remaining two terms ...

## SEM in 1D: A brief summary

$$\int_{\mathsf{E}_{i}} \rho w \ddot{u} dx - \int_{\mathsf{E}_{i}} \mu \left( \frac{\partial}{\partial x} w \right) \left( \frac{\partial}{\partial x} u \right) dx = \int_{\mathsf{E}_{i}} w f dx$$

weak form, element-wise

$$\ddot{\mathbf{u}} = \mathbf{M}^{-1} \cdot (\mathbf{f} - \mathbf{K} \cdot \mathbf{u})$$



# You have survived the math part !



3. The concept in 3D

accurate solutions: discontinuities need to coincide with element boundaries



**low velocities:** short wavelength  $\rightarrow$  small elements

**high velocities:** long wavelength  $\rightarrow$  large elements

many small elements  $\rightarrow$  high computational costs !!!

accurate solutions: discontinuities need to coincide with element boundaries



**low velocities:** short wavelength  $\rightarrow$  small elements

**high velocities:** long wavelength  $\rightarrow$  large elements

## many small elements $\rightarrow$ high computational costs !!!

possible solution: homogenisation theory (Y. Capdeville's talk)

# **Realistic example: The Grenoble valley**



Essentially the same as in 1D:

$$\rho \ddot{u}_{i} - \frac{\partial}{\partial x_{j}} \left( C_{ijkl} * \frac{\partial}{\partial x_{k}} u_{l} \right) = f_{i}$$

- 1. mapping to the reference cube  $[-1, 1]^3$
- 2. polynomial approximation (GLL points)
- 3. numerical integration (GLL quadrature)

$$\ddot{\mathbf{u}} = \mathbf{M}^{-1} \cdot \left( \mathbf{f} - \mathbf{K} \cdot \mathbf{u} \right)$$



deformed element

reference cube



- Interaction with engineering structures
- Nonlinear rheologies (visco-plasticity)



- 2D computational domain makes 3D synthetics
- Spherically symmetric Earth models
- High-frequency wave propagation

See the talk by J. Tromp and Q. Liu.



- Spherical section, regular grid
- Simplistic and very easy to use
- Makes nice tomographic images



Thank you for your attention!