

Using High Frequencies To Improve Low-frequency Inversions

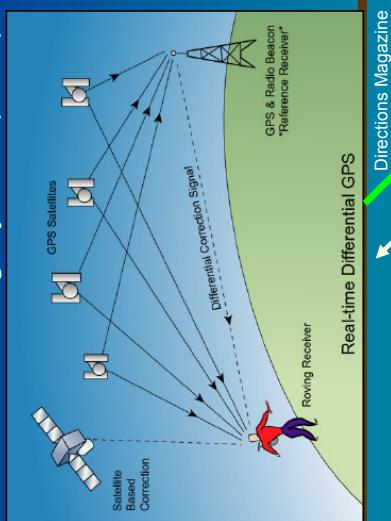
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University of California, Santa Barbara

QUEST: May 20-24, 2013

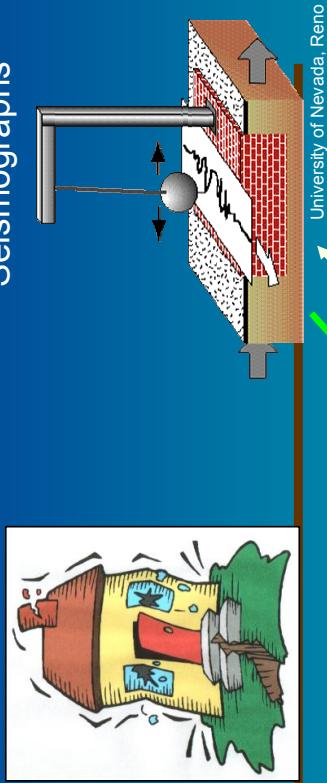
Campus Point, UCSB

Describing the Earthquakes Source: Kinematics

Global Positioning System (GPS)

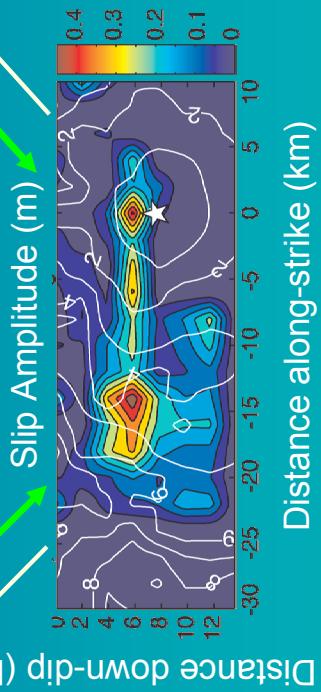


Seismographs



Forward Problem

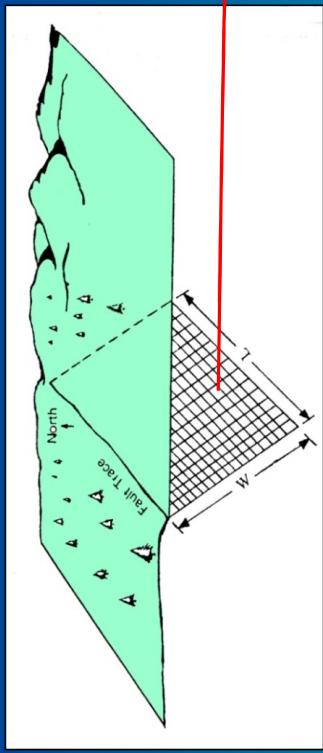
Inverse Problem



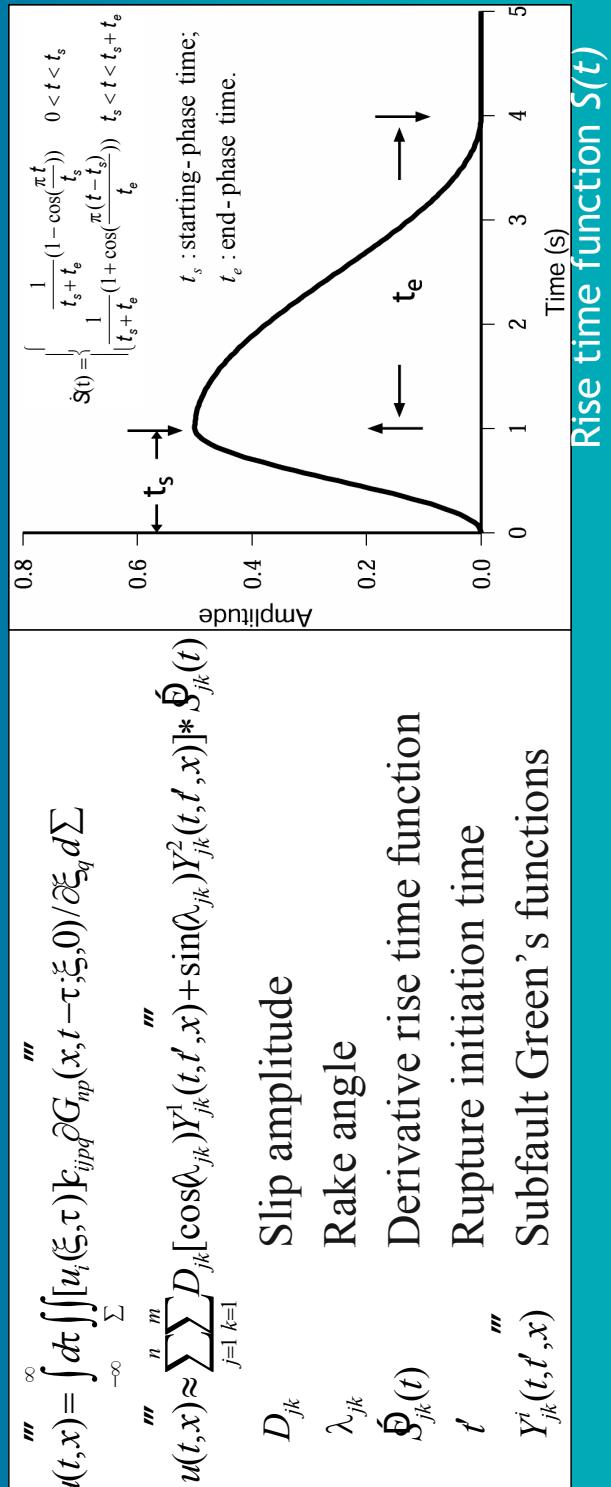
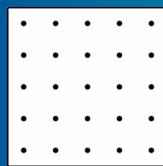
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Courtesy of S. Custódio

Source Representation (Ji et al., 2002, 2003)



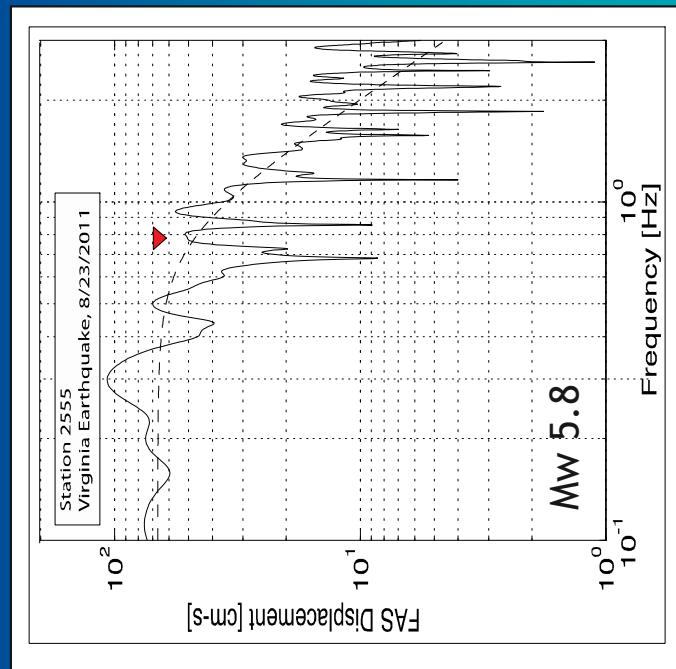
$$Y_{jk}^i(t, t', x) = \sum_p G_{jk}^i(x'_p, x, t) * \delta(t - \Delta t_{jk}^p - t')$$



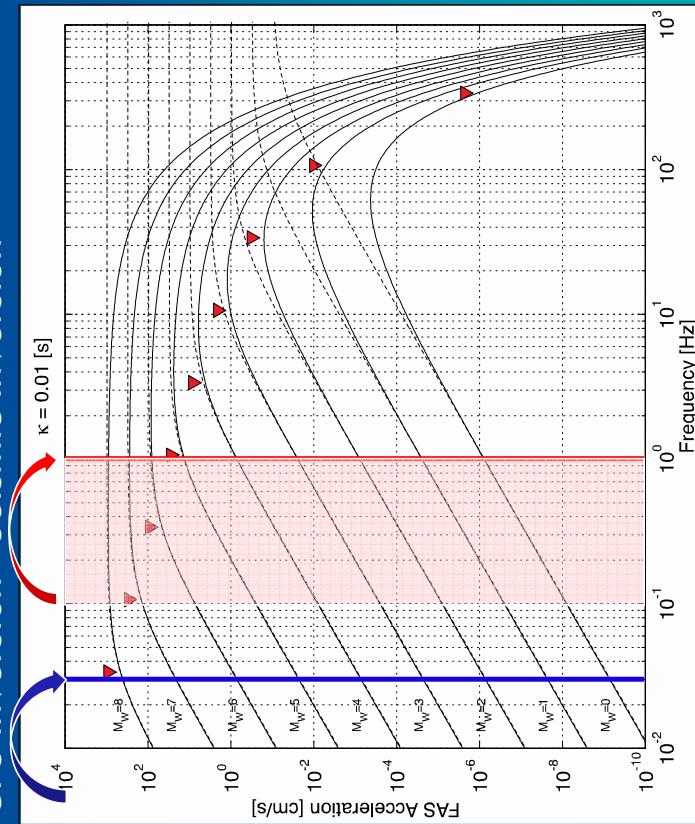
Aki-Brune Acceleration Spectrum

GPS Inversion Seismic Inversion

Displacement Spectrum

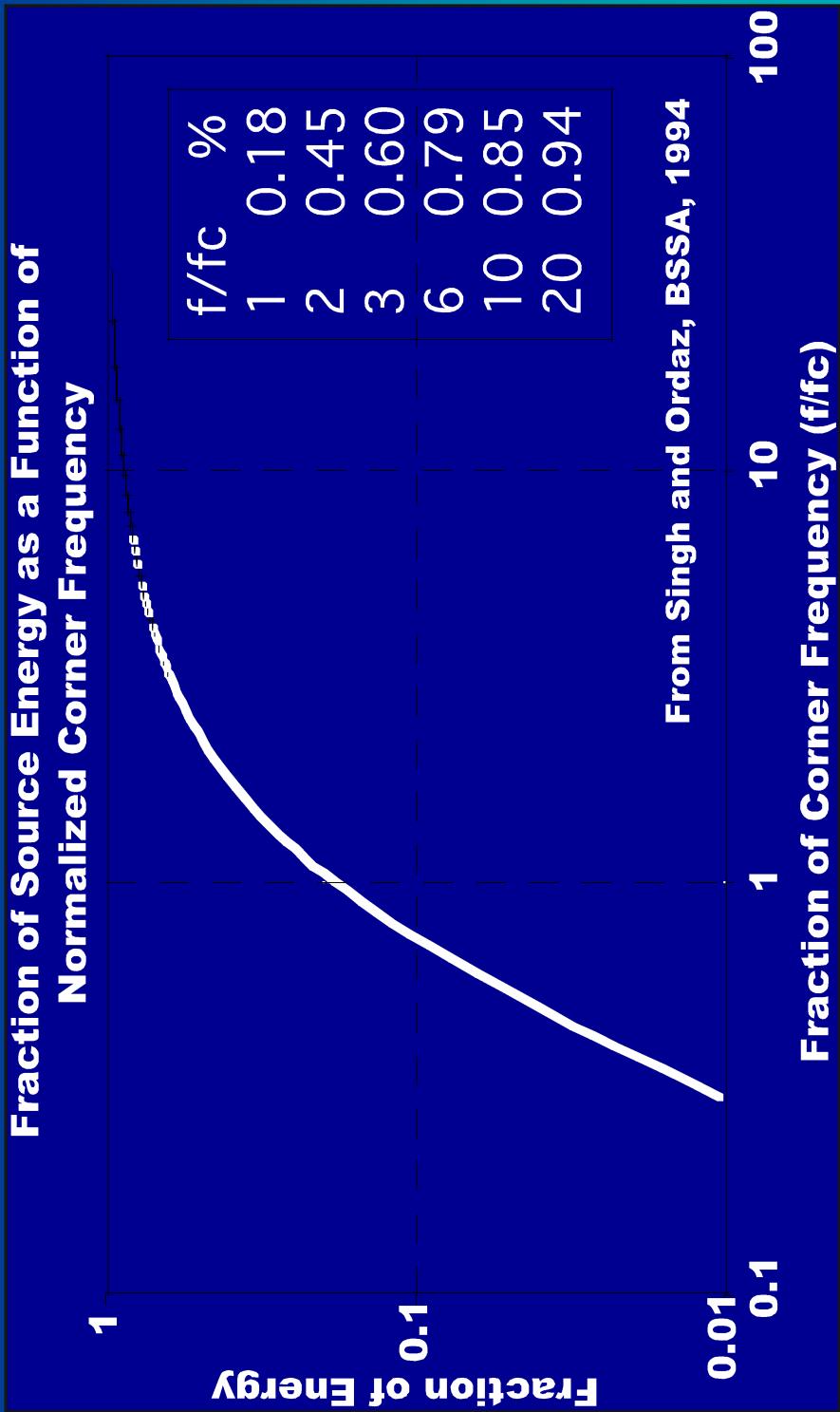


Corner Frequency for $\Delta\sigma=5$ MPa

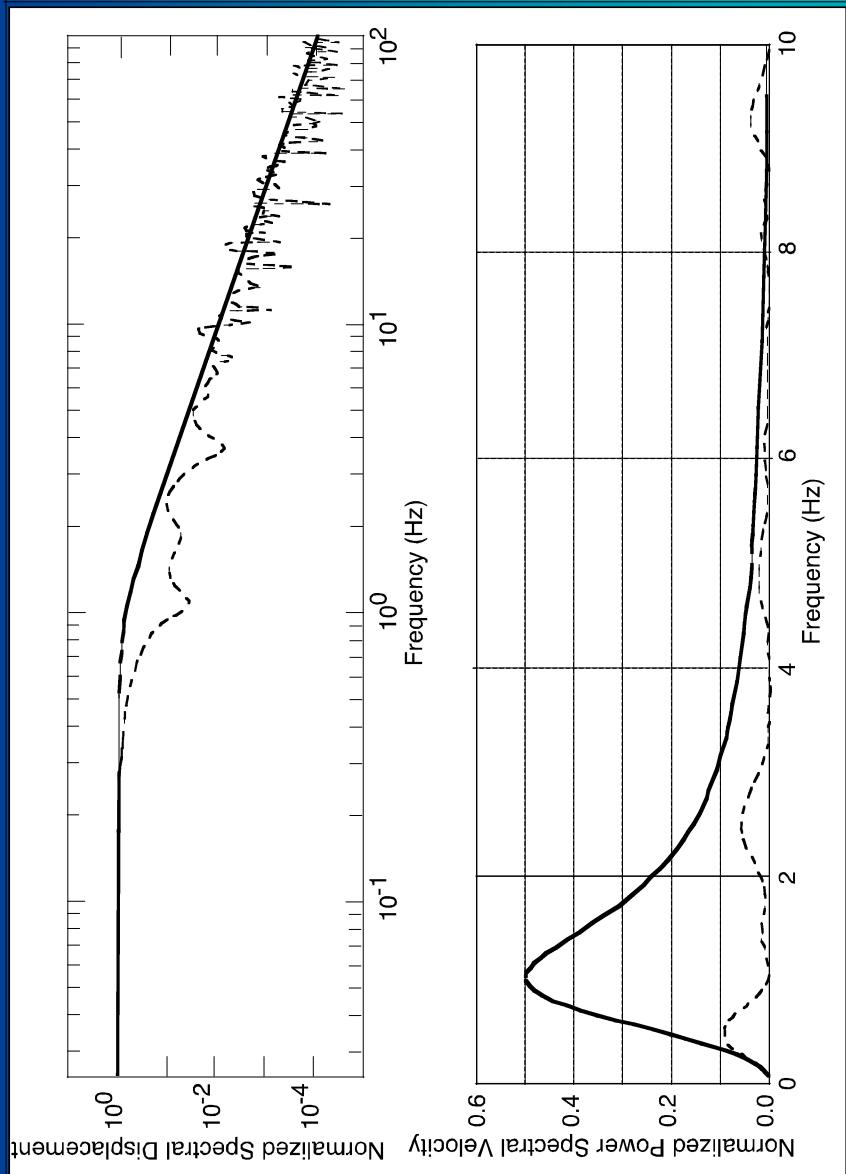


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Energy in Aki-Bruné Spectrum



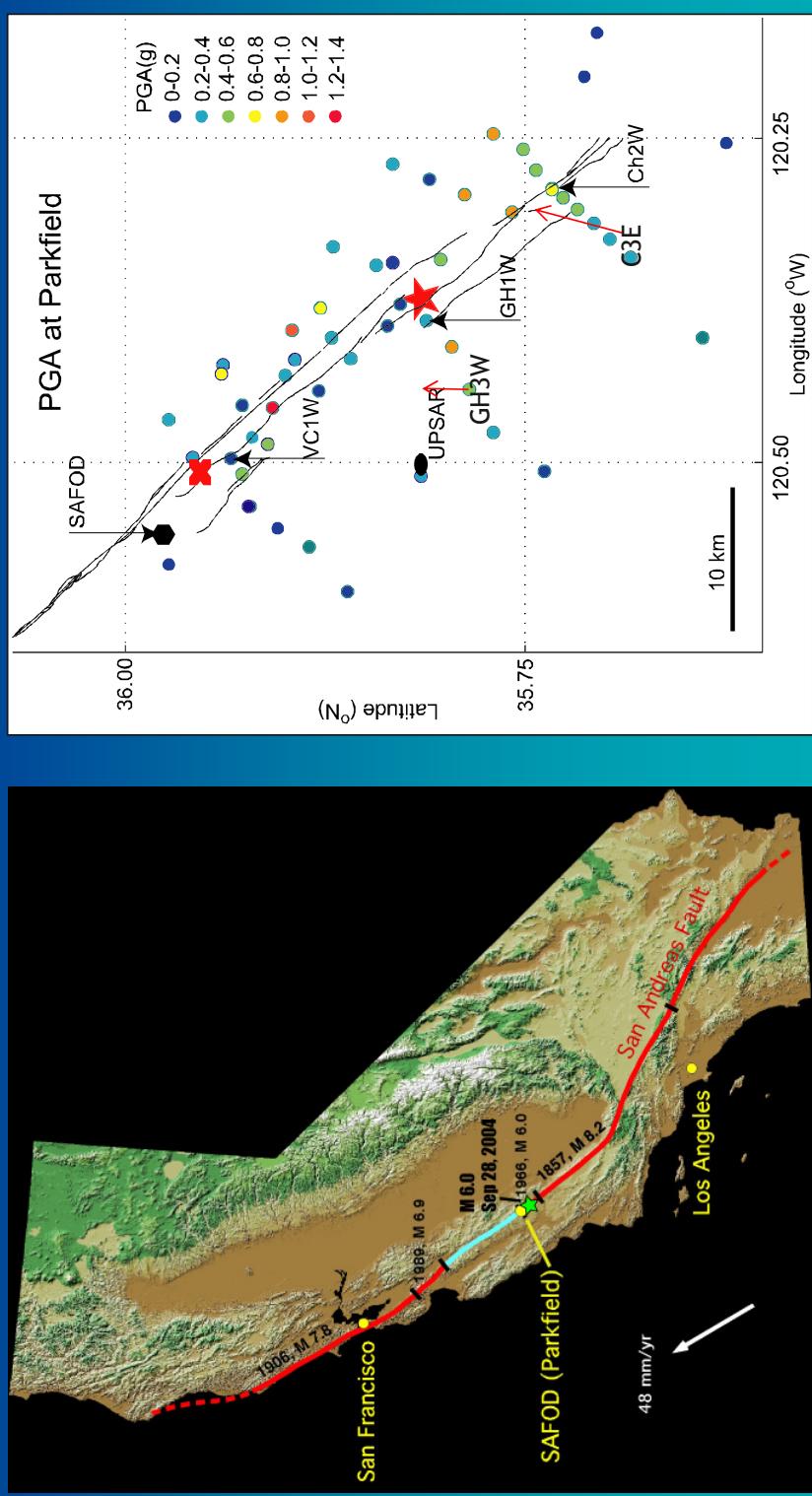
Energy Is Concentrated Near the Corner Frequency



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Tumarkin & Archuleta, 1994

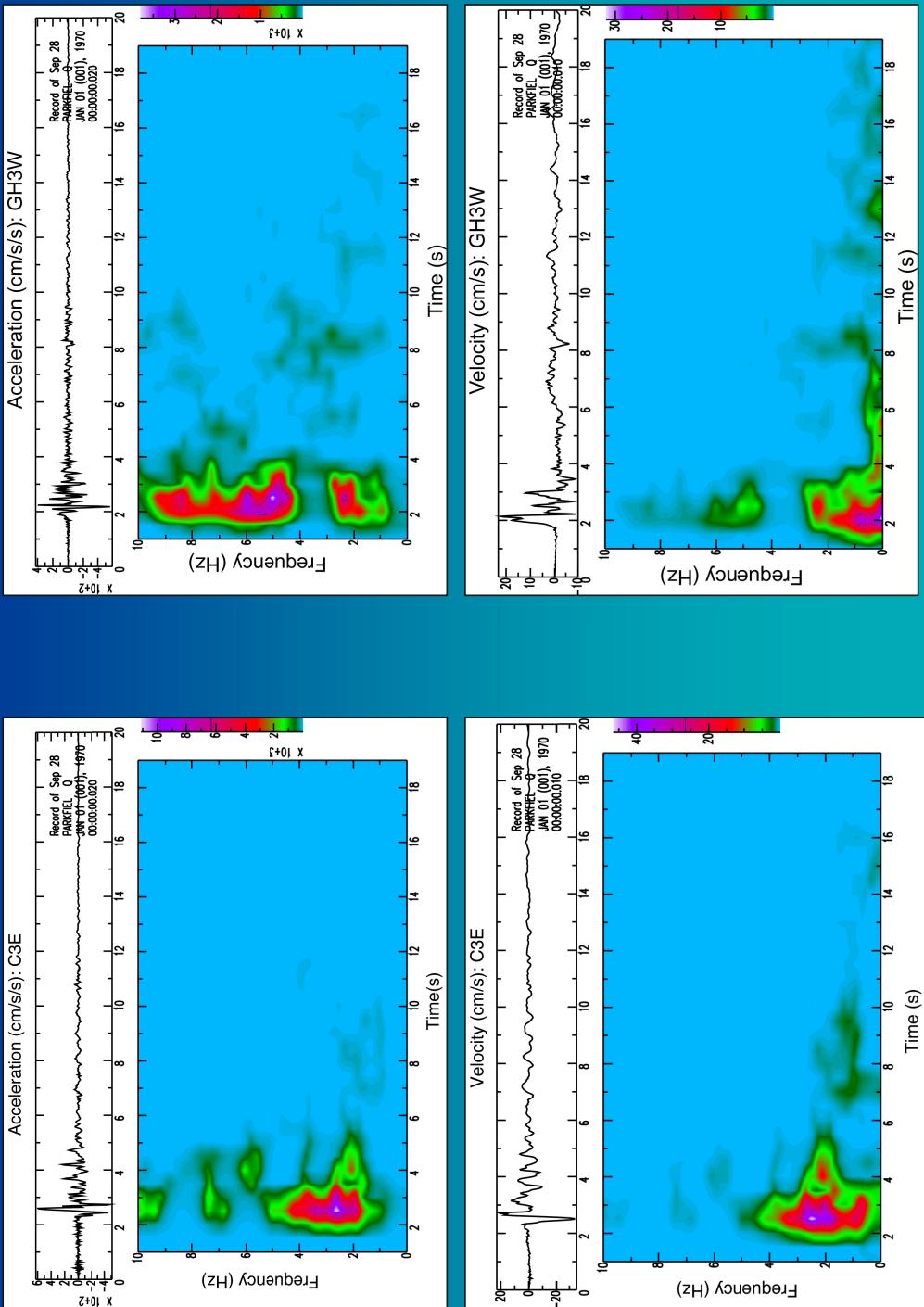
Parkfield Earthquake, M_w 6.0 September 28, 2004



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USGS

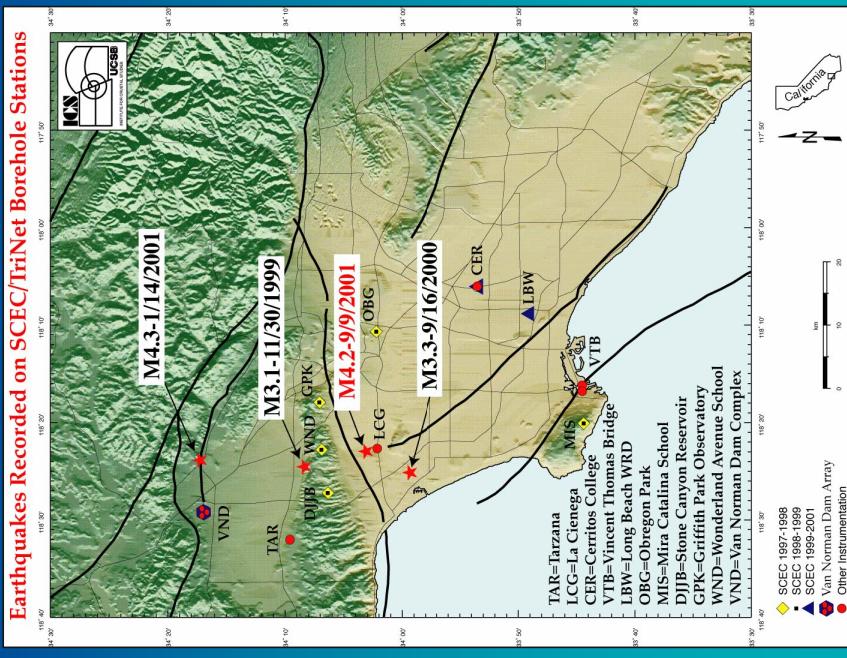
Spectrograms: Station C3E & GH3W



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Courtesy of S. Custódio

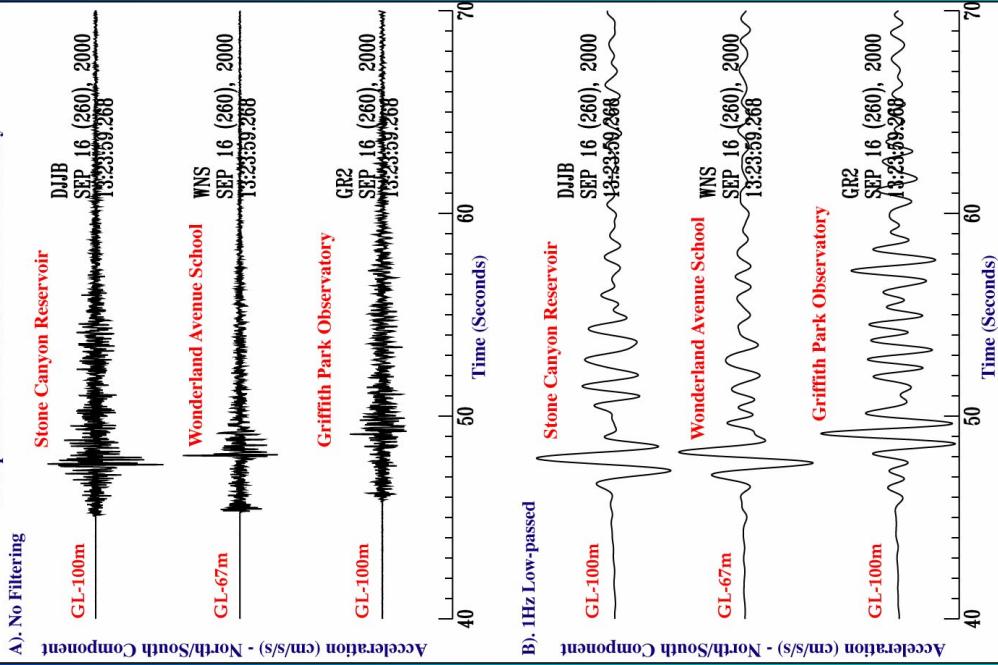
Frequency at which Ground Motion Is Coherent



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At what frequency can we predict ground motions from small earthquakes with simple sources?

Three Borehole Stations Along Santa Monica Mountains
16 September 2000 M3.3 Near Marina Del Rey



Courtesy of Jamie Steidl

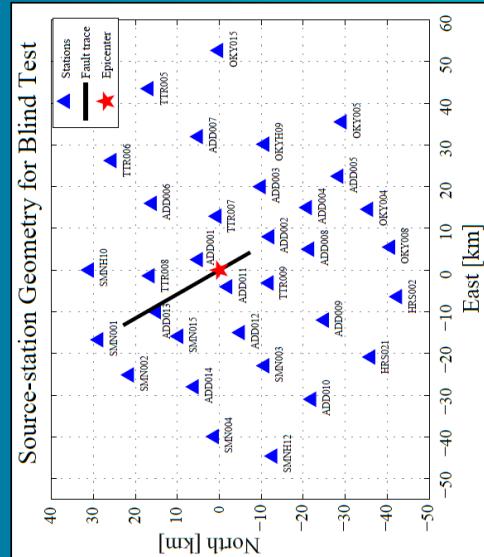
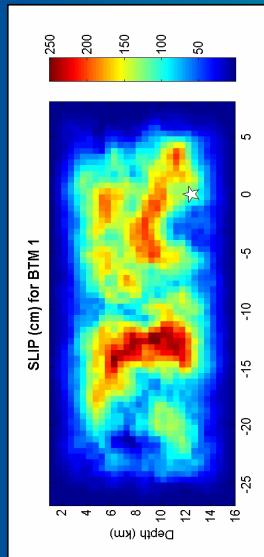
SPICE BlindTest I (Mai et al., 2007)

- **Data**
 - 1: Seismic data in velocity ($f_{max} \sim 3$ Hz)
 - 2: Static displacements

- **Available information**

- 1: Fault geometry & Hypocentral location
(strike, dip, rake: 150° , 90° , 0°)
- 2: Total seismic moment:
 1.43×10^{26} dyne-cm
- 3: Velocity structure
- 4: Rupture does not break the surface

Input model

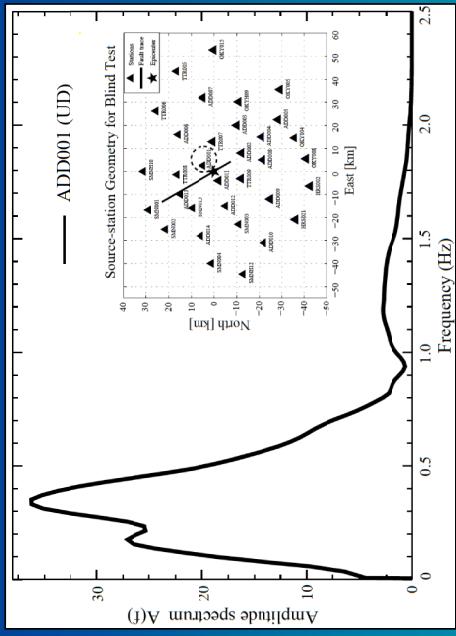


- **To be resolved:**

1. Slip distribution on the fault plane
2. Rupture velocity & rise time (both are constant; the investigators were given this information but not the values)

BlindTest website: <http://www.seismo.ethz.ch/staff/martin/BlindTTest.html>
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Spectrum: Energy Ratio



Average relative energy

$$\overline{R}^b = \frac{100}{N} \sum_{i=1}^N \frac{\int (o_i^b(t))^2 dt}{\int (o_i(t))^2 dt}$$

Relative Energy			
0-2.0 (Hz)	0-0.1 (Hz)	0.1-1.0 (Hz)	1.0-2.0 (Hz)
100%	15.04%	86.02%	2.73%

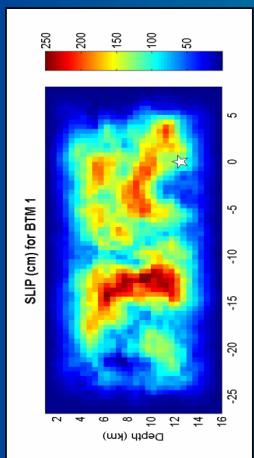
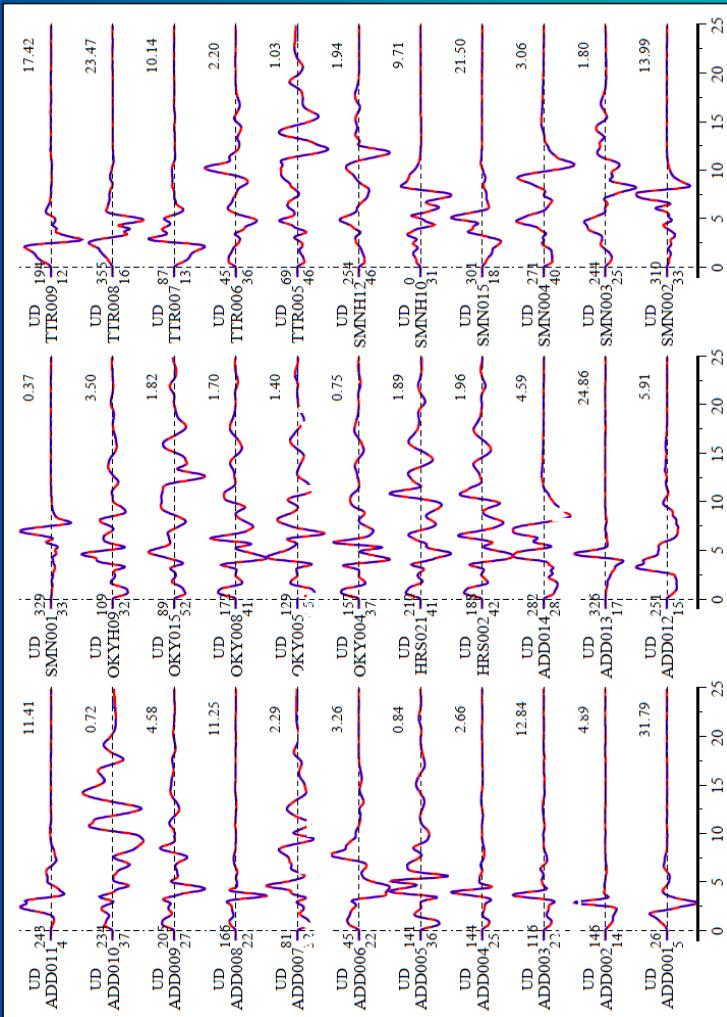
Note:

Misfit functions, such as variance reduction, are designed to catch the difference in amplitude (or energy). Therefore, for this case, it is dominated by the signals from 0.1 to 1 Hz.

Forward Calculation

Input model

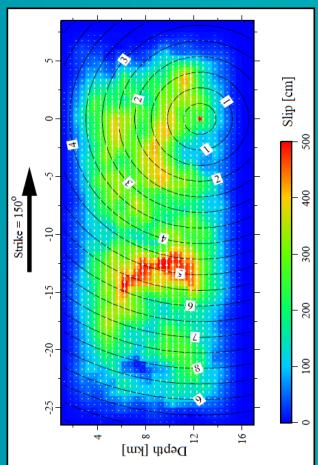
Vertical components in velocity



Corrected data

Double of our
synthetics

↓ Target



Shao & Ji, GJI 2012

Indistinguishable visually !

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Variance Reduction

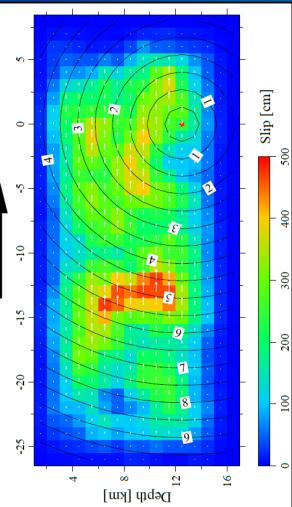
Variance Reduction Function

$$\bar{V}^b = \frac{1}{N} \sum_{i=1}^N \frac{\int (o_i^b(t) - s_i^b(t))^2 dt}{\int (o_i^b(t))^2 dt}$$

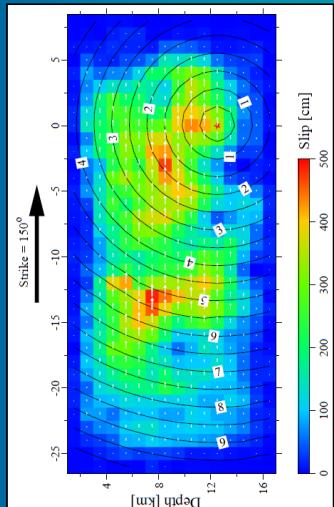
b denotes a bandpass filter

Variance reductions			
0-2.0 (Hz)	0-0.1 (Hz)	0.1-1.0 (Hz)	1.0-2.0 (Hz)
99.91%	99.98%	99.92%	97.53%

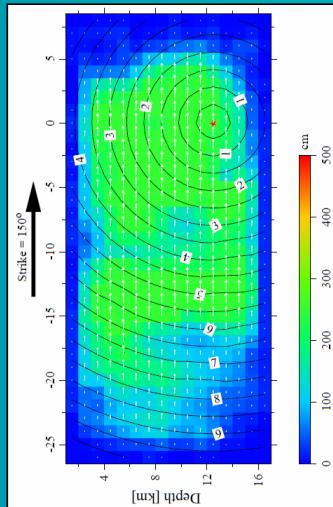
Target_SC



Model I



Model III



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Variance Reduction: 3 Models

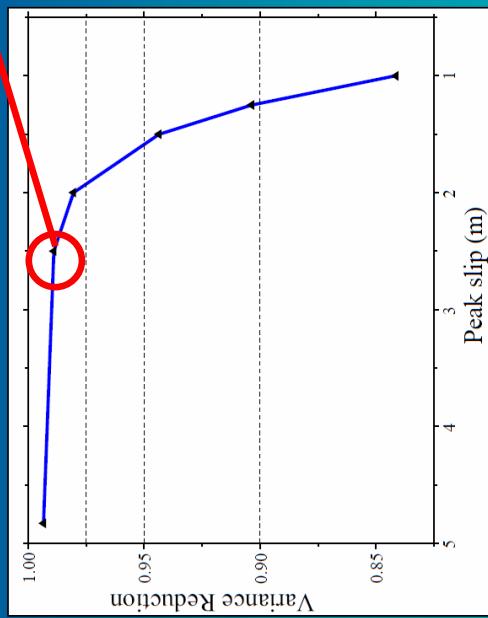
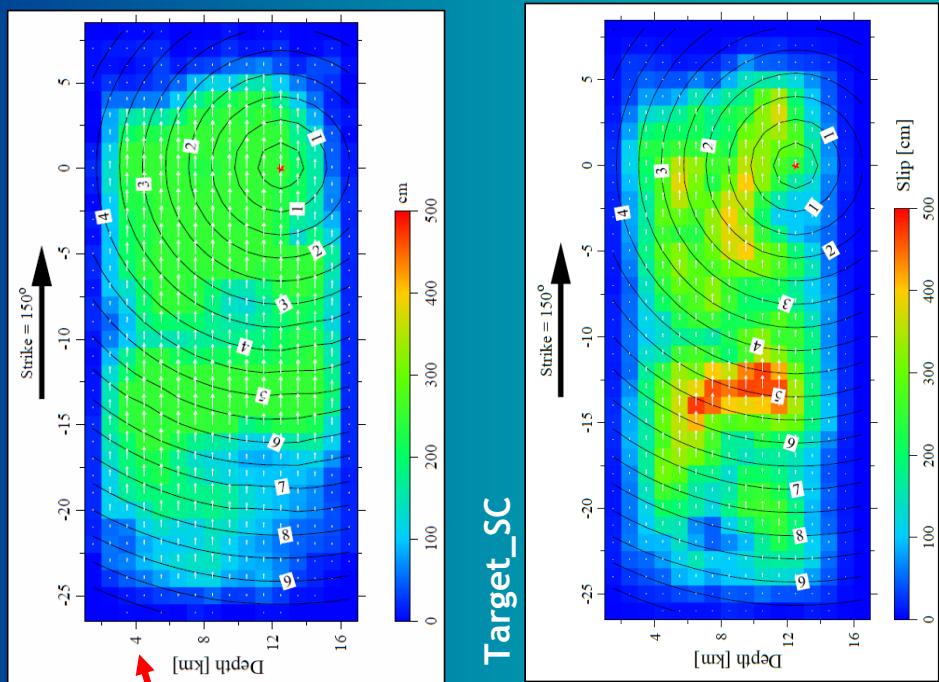
Models	Variance reductions			
	0-2.0 (Hz)	0-0.1 (Hz)	0.1-1.0 (Hz)	1.0-2.0 (Hz)
Target_SC	99.32%	99.72%	99.45%	86.21%
Model I	99.35%	99.28%	99.61%	77.02%
Model III	98.87%	98.90%	99.36%	64.26%

Model III cannot match the signals from 1 to 2 Hz.

Shao & Ji, GJI 2012

Sensitivity Test: Peak Slip

Model III: Peak slip = 2.5 m



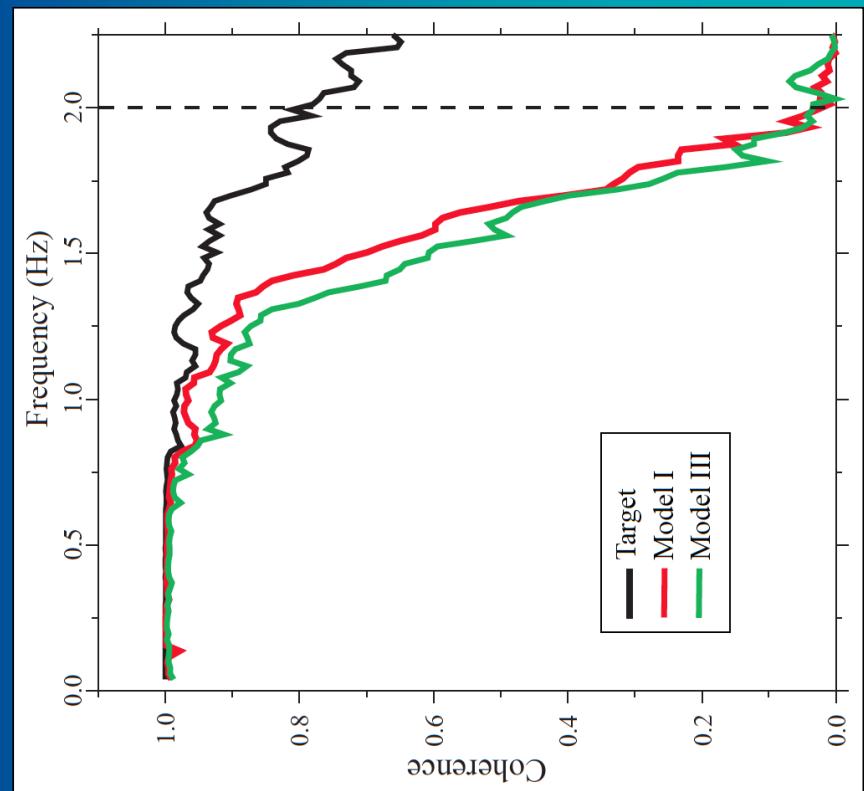
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Shao & Ji, GJI 2012

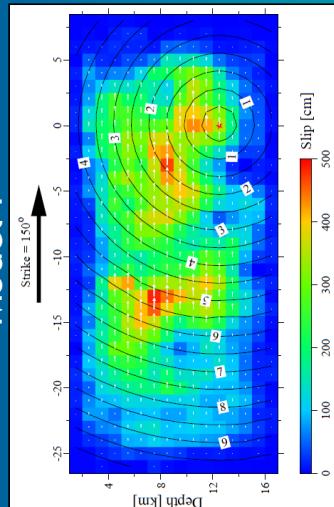
“Coherence” Function

High frequency signals are sensitive to the details of the slip models.

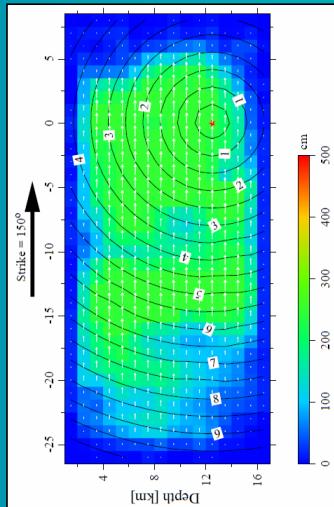
$$e(f) = \frac{1}{N} \left| \sum_i^N \frac{2 \operatorname{REAL}[d_i(f) s_i^*(f)]}{d_i(f) d_i^*(f) + s_i(f) s_i^*(f)} \right|$$



Model I



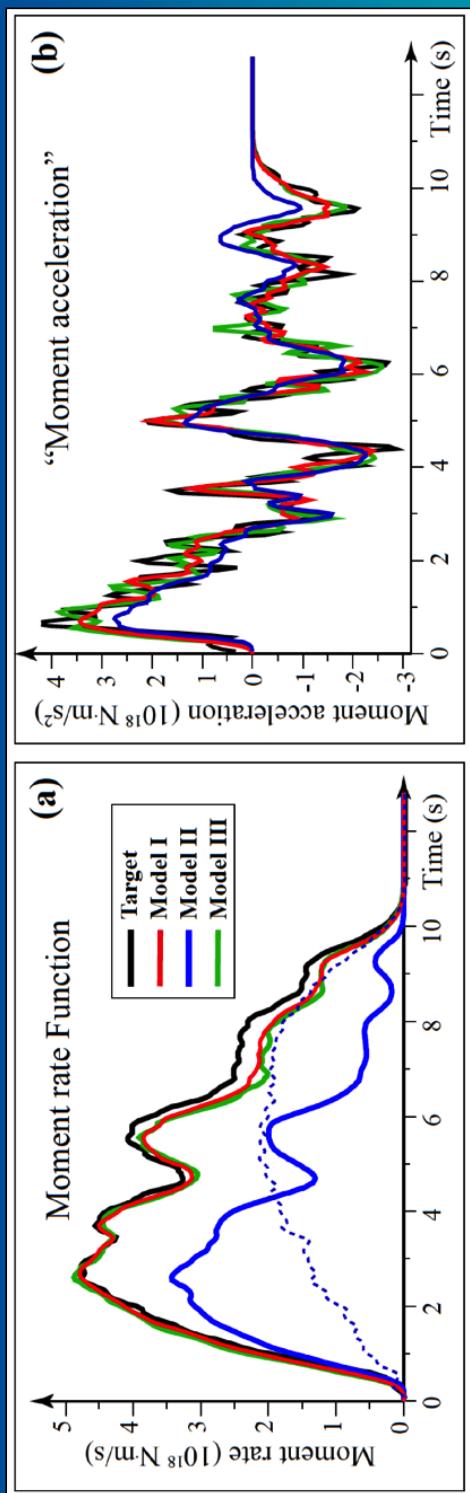
Model III



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Shao & Ji, GJI 2012

Comparing Moment Rate Functions



Far field body-wave

1: Displacement

$$U(r, t) \approx \frac{1}{4\pi\rho v^3} \psi(\theta, \phi) \frac{1}{r} \hat{M}(t)$$

2: Velocity

$$V(r, t) \approx \frac{1}{4\pi\rho v^3} \psi(\theta, \phi) \frac{1}{r} \tilde{\hat{M}}(t)$$

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Shao & Ji, GJI 2012

Back-projection

Suppose the excited ground motion at the i -th station can be repre

$$\mathbf{s}_i(t) = \sum_{j=1}^N M_o^j(t) * W_i^j(t)$$

For the j -th subevent, we can define simple back-propagation function (SBP) and network response function (NRF) as

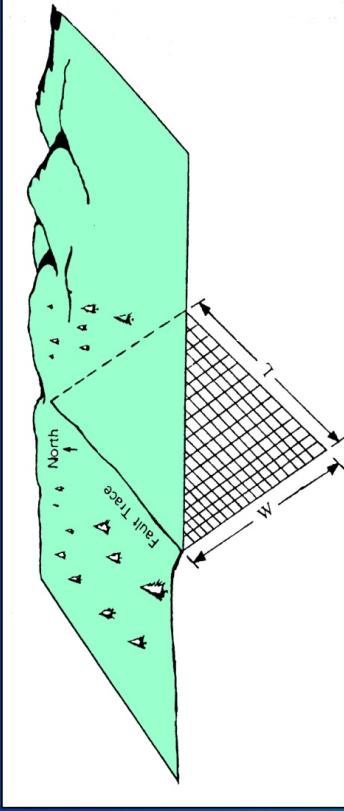
$$\frac{sbp_j(t) = \sum_{i=1}^L s_i(t) * W_i^j(-t)}{nrf_j(t) = \sum_{i=1}^L W_i^j(t) * W_i^j(-t)}$$

It is straightforward to prove

$$mbf_j(t) = M_o^j(t) + \sum_{k \neq j}^N M_o^k(t) * \left[\sum_{i=1}^L W_i^k(t) * W_i^j(-t) \right] *^{-1} nrf_j(t)$$

*Imaging error caused by the slip on
the rest of fault plane*

L stations

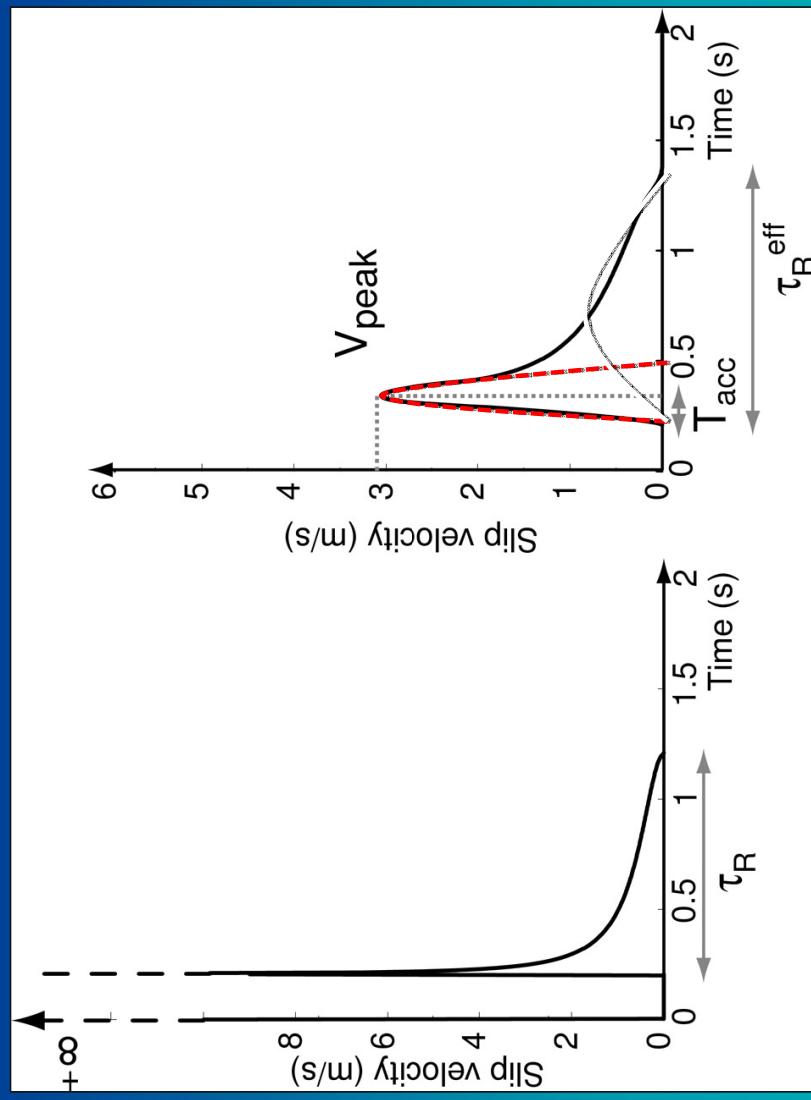


$$mbf_j(t) = sbp_j(t) *^{-1} nrf_j(t)$$

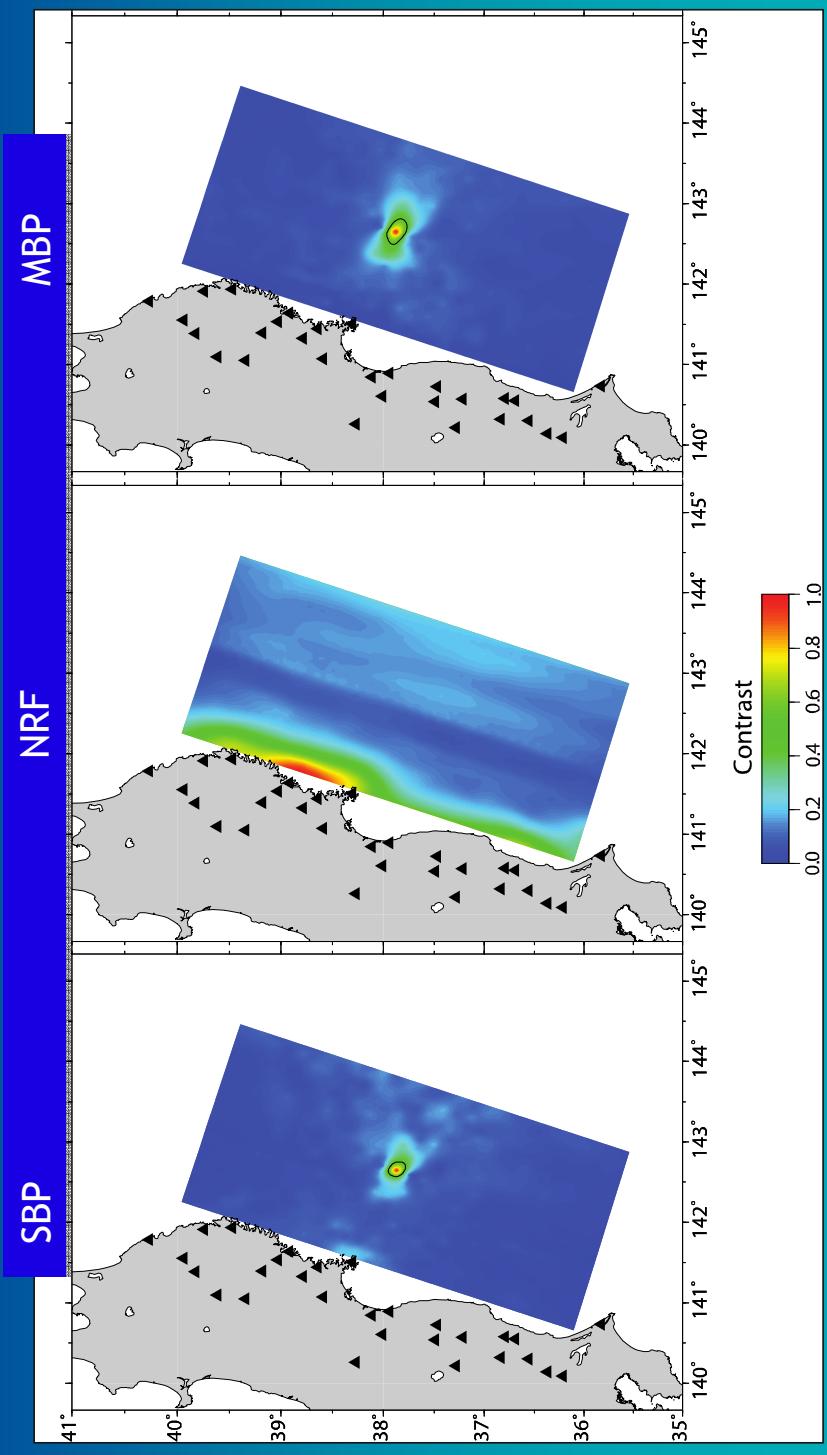
Modified back-projection function (MBF)

Slip rate function

As the high frequency radiation is mainly caused by the initial rupture, we assume the target subevent has a 0.8 s triangular slip rate function.



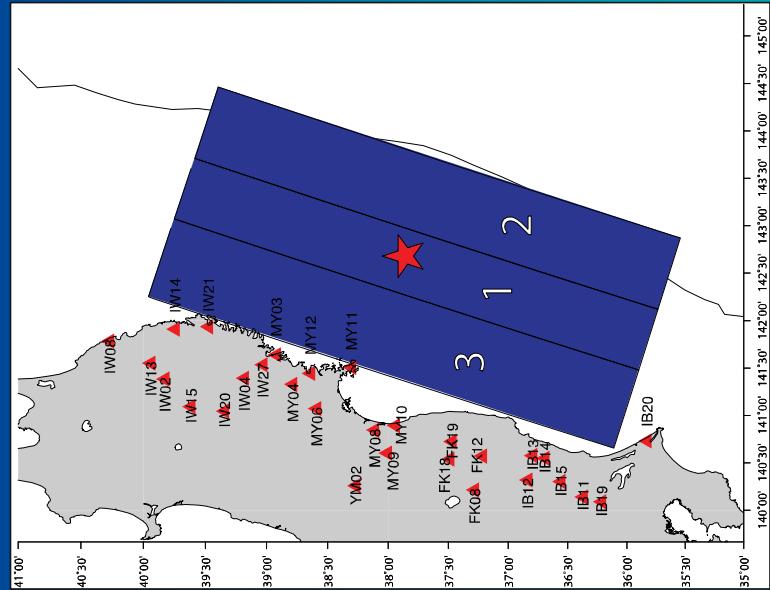
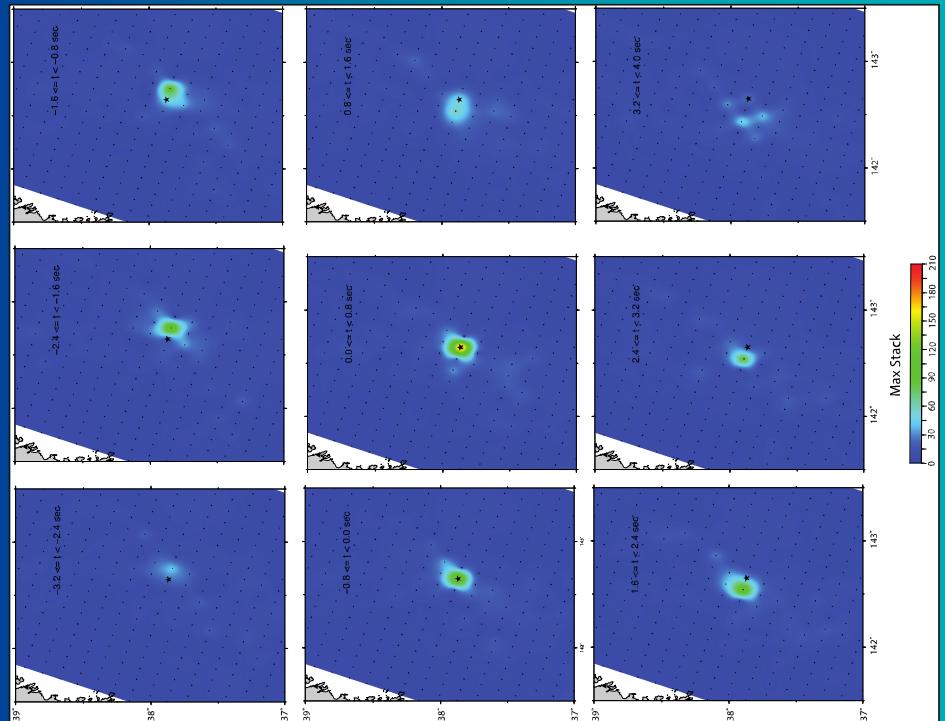
Comparison of Back-projection Functions and Network Response Function



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[Yano, 2012]

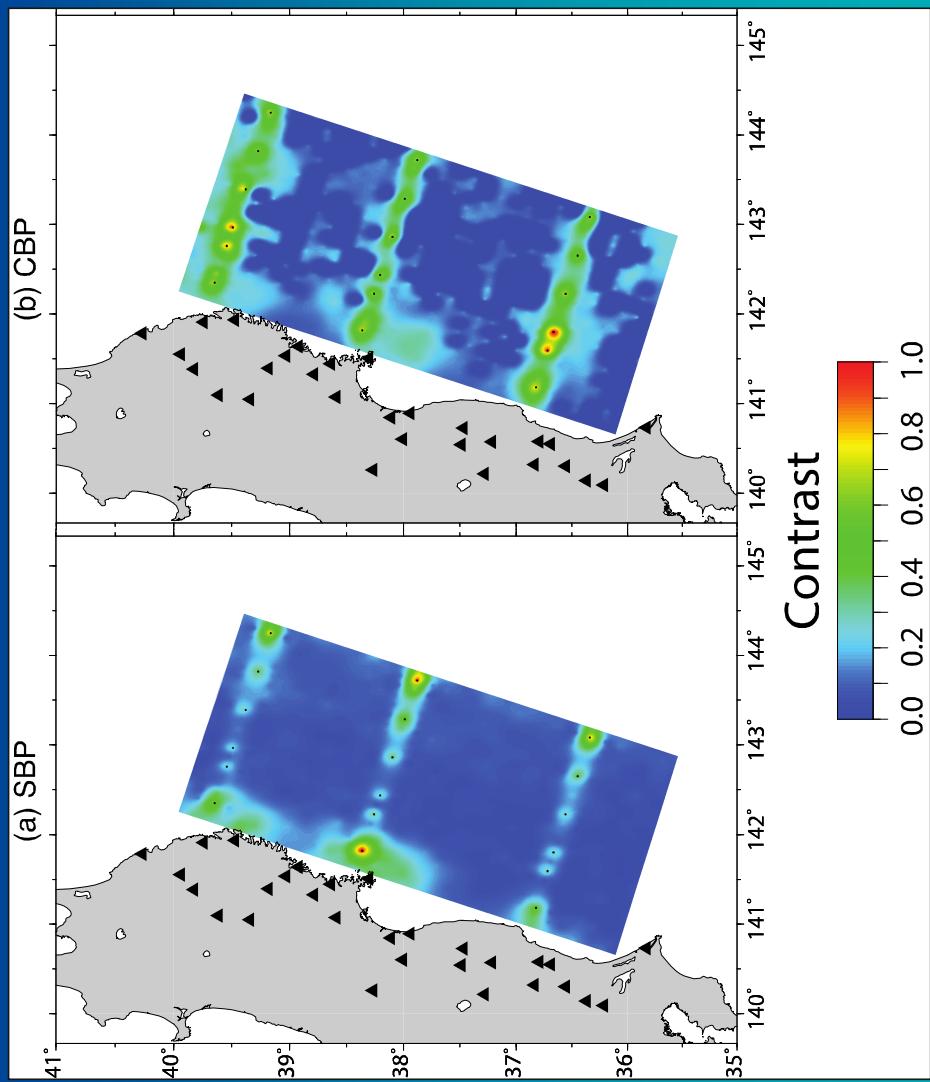
Numerical Test: Effect of Station Distribution



QUEST: May20-24, 2013

[Yano, 2012]

Numerical Test



QUEST: May20-24, 2013

[Yano, 2012]

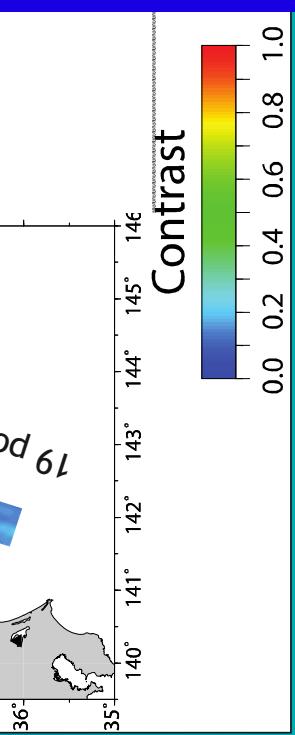
Back-projection

Synthetic Observations:

18 uniformly distributed stations on one side. Such a station distribution has relatively lower spatial resolution in down-dip direction but shall be optimal to track along strike rupture.

Target sources:

19 point sources distribute along a line with 15 km interval. A constant 0.8 s triangular slip rate function. Rupture propagation with a speed of 1.5 km/s.

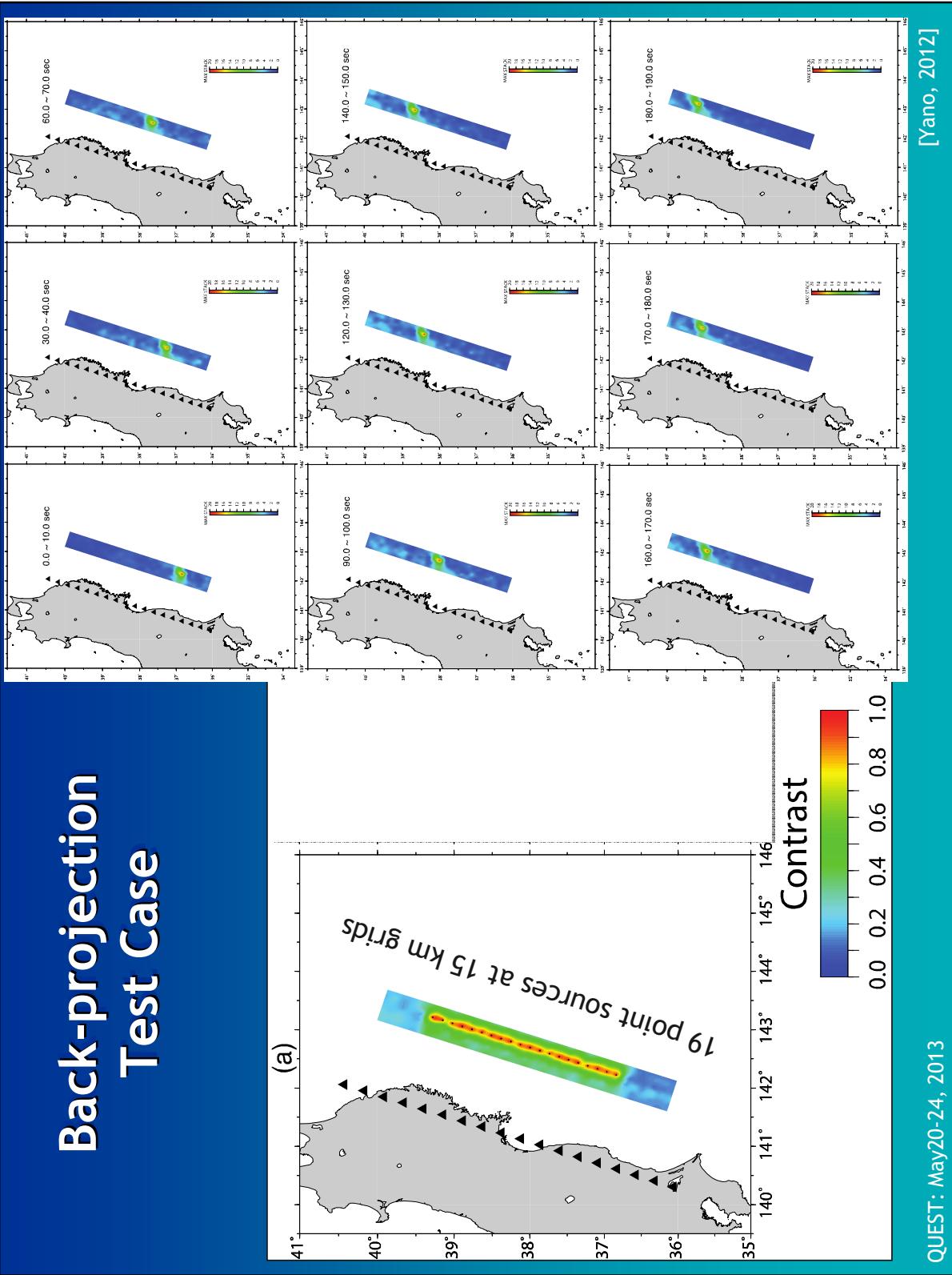


The data has been bandpass filtered from 0.03 Hz to 1 Hz before this back-propagation analysis

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[Yano, 2012]

Back-projection Test Case



Back-Projection

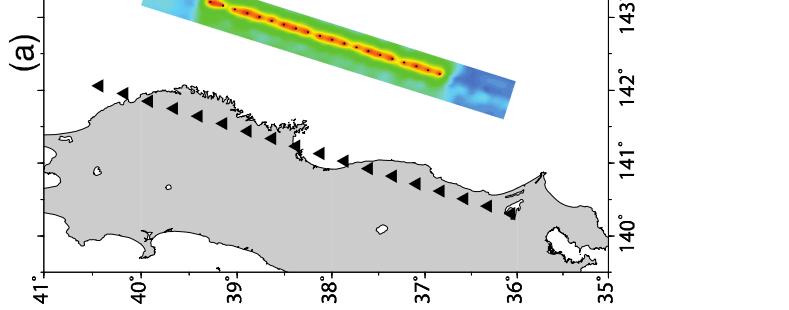
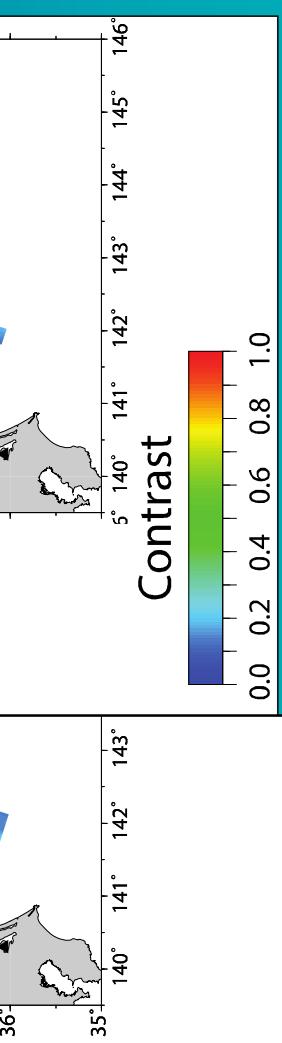
[Yano et al., 2012]

Synthetic Observations:

18 uniformly distributed stations on one side. Such a station distribution has relatively lower spatial resolution in down-dip direction but shall be optimal to track along strike rupture.

Target sources:

270 point sources distribute along a line with 1 km interval. A constant 0.8 s triangular slip rate function. Unilateral rupture with a velocity of 1.5 km/s.

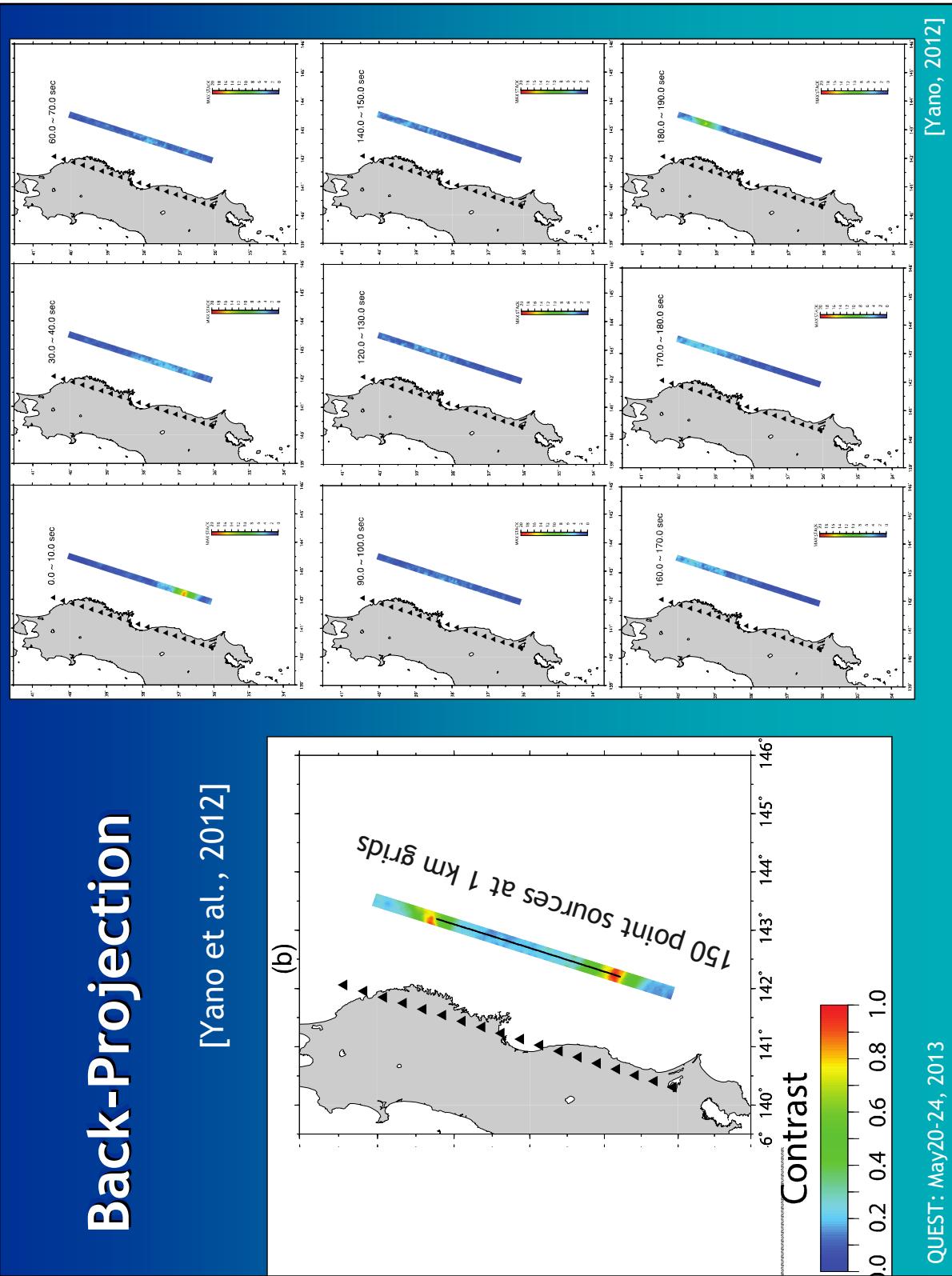


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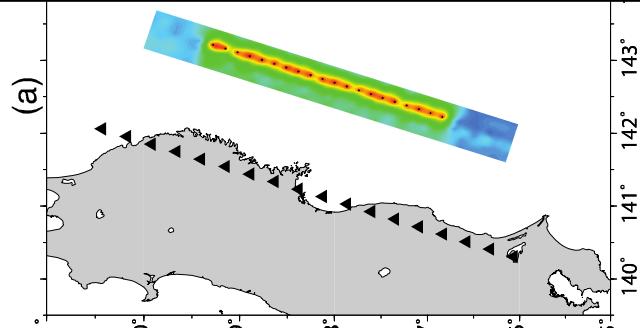
[Yano, 2012]

Back-Projection

[Yano et al., 2012]

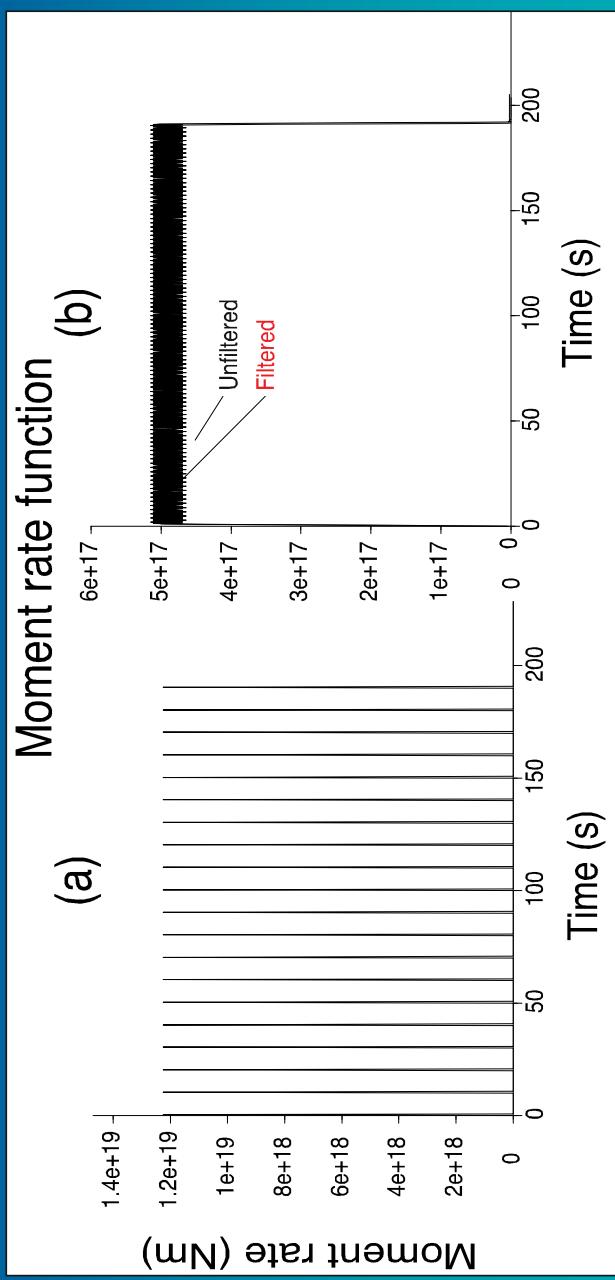


(a)



Comparison of Moment Rate Functions

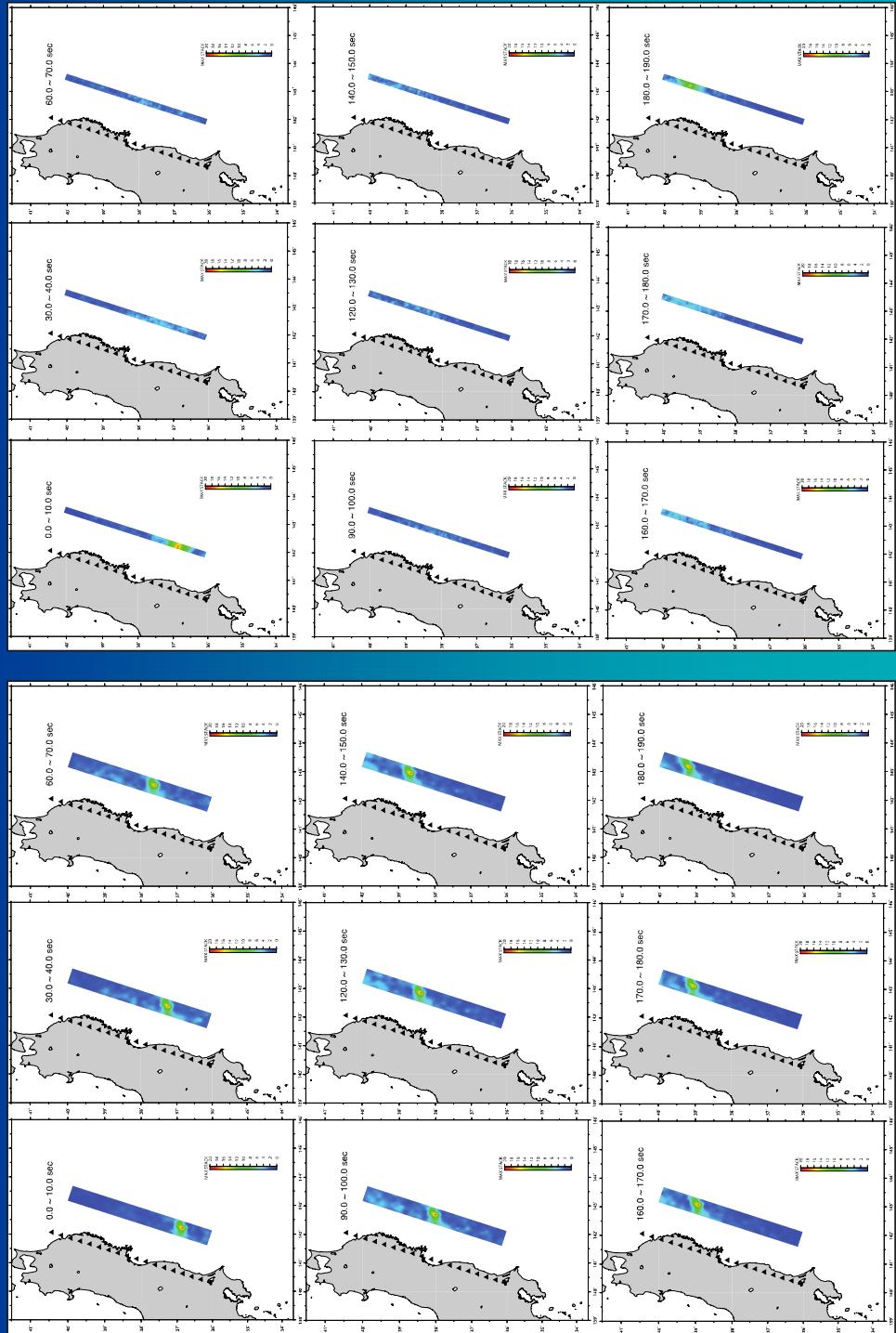
15 km interval target sources 1 km interval target sources



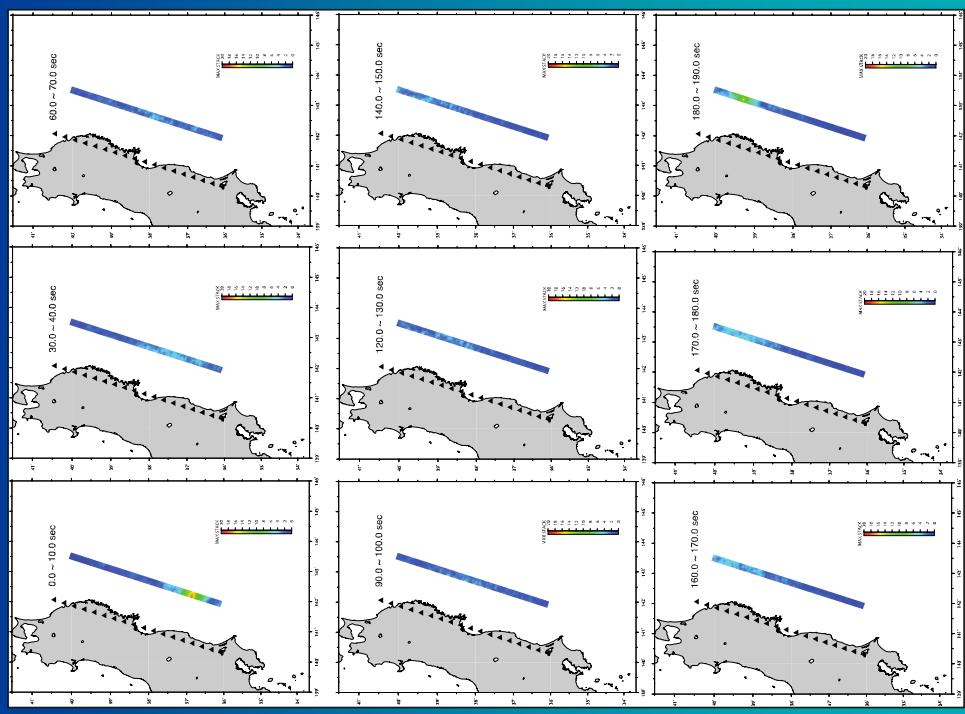
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[Yano, 2012]

Target sources at 15 km intervals



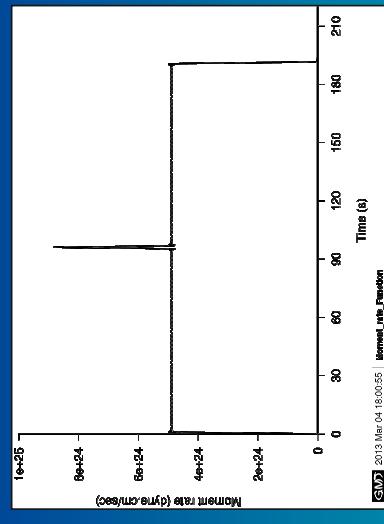
Target sources at 1.0 km intervals



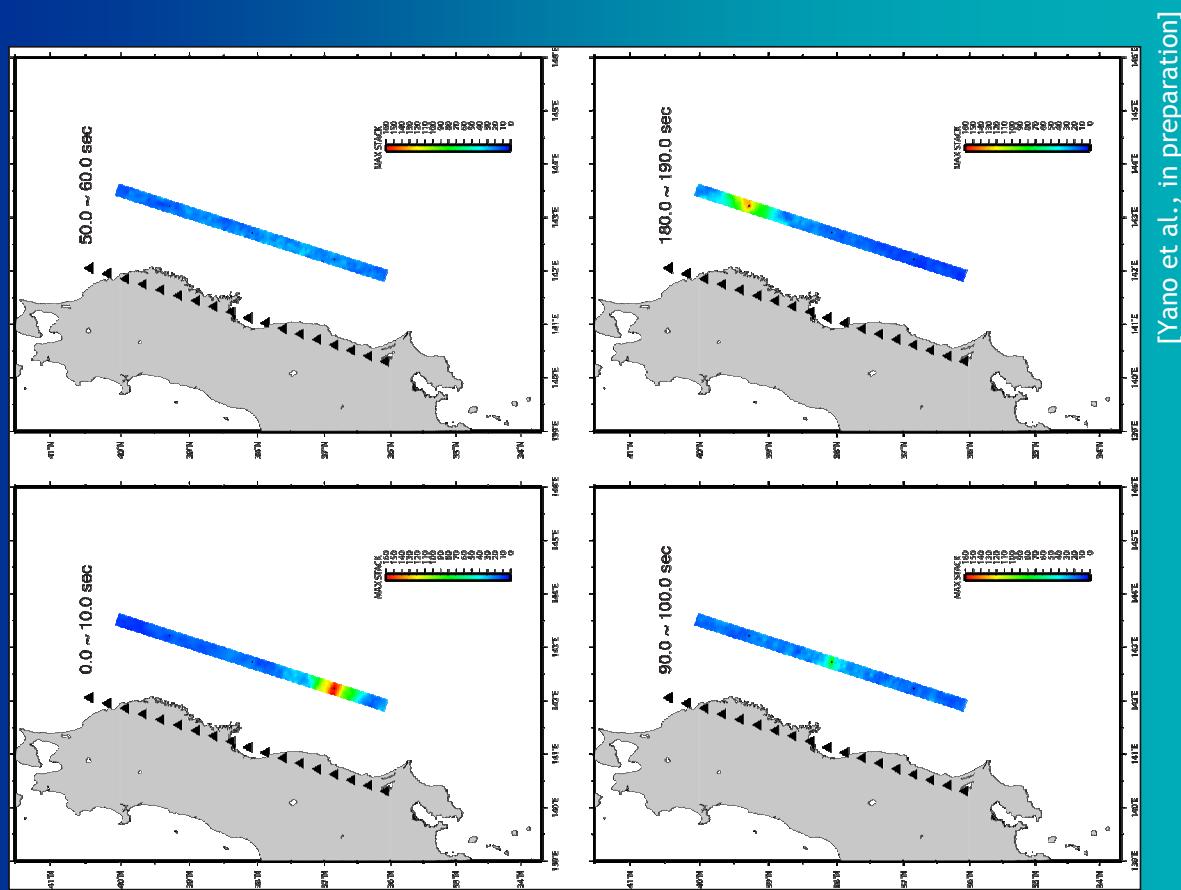
QUEST: May20-24, 2013

[Yano, 2012]

Single Variation in Moment Rate

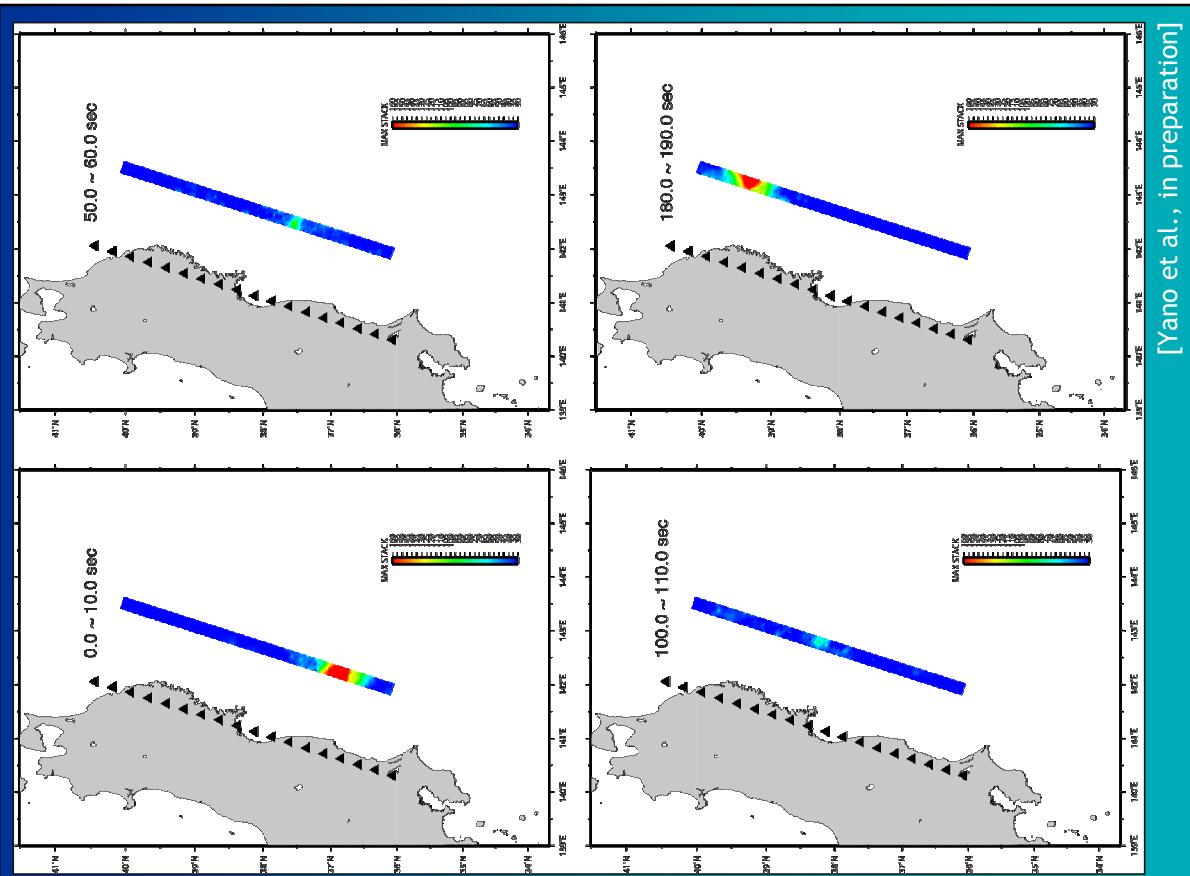
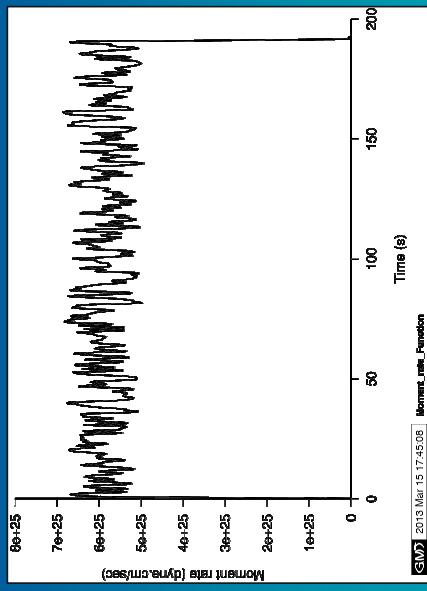


While the back projection can determine the location of the single point that varies, the amplitude is proportional only to the height above the constant moment rate. Compare beginning and ending points with the point in the middle.



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Variation in Moment Rate



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[Yano et al., in preparation]

Conclusions

- ❖ Waveform inversion may not be an effective means to determine small scale variations of the faulting.
- ❖ The variations in the moment rate function may shed light on the basic heterogeneity of the faulting.
- ❖ Back-projection analysis is good to resolve the high frequency radiation from isolated sources. But for continuous rupture, high frequency radiation captured by the back-projection analyses generally does not have a one to one relationship with the true high frequency radiation from an individual slip patch.
- ❖ The fact that rupture front of large earthquakes can be imaged by back-projection analysis implies that rupture propagation is heterogeneous.